



# 非晶态合金在催化领域的应用

吴用, 余鹏\*

重庆师范大学物理与电子工程学院, 重庆 401331

\*联系人, E-mail: pengyu@cqu.edu.cn

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**摘要** 非晶态合金具有长程无序、短程有序的独特原子结构, 表现出一系列优异的力学、物理和化学性能. 近年来, 非晶态合金在催化领域的研究和应用受到了广泛关注. 与晶态结构相比, 非晶态结构具有不饱和位点多、潜在的吸附容量更大、耐腐蚀性好等优点. 无晶格、晶界和位错的限制使得其组分和电子结构具有更大的调控范围, 有利于最大程度提升合金的催化活性. 本文简要综述了非晶态合金催化剂的发展历程、结构优势以及在催化领域的应用潜力, 同时总结了其面临的挑战和应用前景.

**关键词** 非晶态合金, 催化剂, 性能优势, 应用前景

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## 1 非晶态合金催化剂的发展历程

非晶态合金的研究始于20世纪<sup>[1]</sup>, 1950年Brenner等人<sup>[2]</sup>采用电沉积法成功制备了Ni-P非晶态合金, 随后Ni-P非晶态合金镀层被广泛应用于金属表面的防护涂层, 这标志着非晶态合金的首次工业应用. 1959年, Cohen和Turnbull<sup>[3]</sup>提出了非晶态合金的形成理论, 为非晶态合金及其物理特性的研究奠定了基础. 1960年, Klement Jun.等人<sup>[4]</sup>通过熔体淬火技术制备了二元Au-Si非晶态合金, 标志着非晶态合金研究的新纪元. 自1960年以来, 非晶态合金的种类不断增加, 展现出多种特性<sup>[5]</sup>. 与晶态合金相比, 非晶态合金不仅具有金属特性, 还展现出许多与非晶态结构相关的独特性质, 成为理想的结构功能材料<sup>[6-8]</sup>.

非晶态合金作为新型催化材料的研究始于1980年. Smith等人<sup>[9]</sup>在第七届国际催化会议上报道了关于非晶态合金作为催化剂的工作, 促进了非晶态合金在催化领域的迅速发展<sup>[10]</sup>. 1986年, van Wonerghem等人<sup>[11]</sup>使用化学还原法制备了超微非晶态合金粒子, 将“超微粒子”与“非晶态”两个概念结合在一起, 进一步推动了非晶态合金在催化领域的发展(图1)<sup>[12-21]</sup>. 20世纪80年代中期, 在闵恩泽的带领下, 中国石油化工股份有限公司石油化工科学研究院联合中石化生产企业和相关高校, 开始进行非晶态合金和磁稳定床反应工程技术的基础研究. 通过催化材料和反应工程的创新集成, 实现了跨越式发展, 并取得了重大经济和社会效益. 历经20年研发的“非晶态合金催化剂和磁稳定床反应工艺的创新与集成”项目, 荣获2005年国家技术发明

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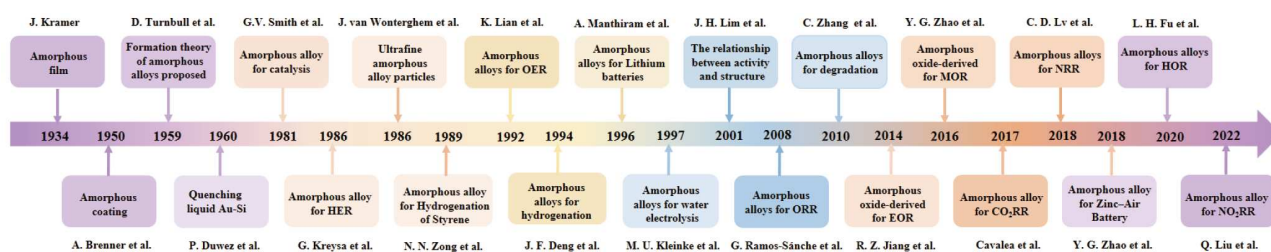


图 1 (网络版彩图)非晶态合金在催化领域的发展历程

Figure 1 (Color online) The development of amorphous alloy in the catalysis fields.

一等奖和2007年国家最高科学技术奖。

近年来, 非晶态合金催化剂在催化领域受到越来越多的关注, 在还原反应催化(包括析氢反应(HER)和氧还原反应(ORR)等)、氧化反应催化(包括析氧反应(OER)、醇氧化反应(AOR)和尿素氧化反应(UOR)等)以及污水处理等方面均取得了阶段性的重要进展. 本文简要综述了非晶态合金催化剂在催化领域的应用, 为设计高活性、高稳定性的非晶态合金催化剂提供参考.

## 2 非晶态合金催化剂的结构优势

与稳定的晶态结构相比, 非晶态合金被认为是亚稳的过渡中间态<sup>[22,23]</sup>. 它们类似液体的无序原子排列, 使非晶态合金看起来像是“冻结”的无序固体(图2)<sup>[7,24]</sup>. 长期以来, 人们主要关注各种晶体材料的结构和性能, 对非晶态合金的结构特征和性能研究仍处于探索阶段, 没有形成固定的研究范式. 因此, 尽管对非晶态合金的研究已有近百年, 但目前对非晶态合金催化剂的研究仍处于初步探索阶段<sup>[25]</sup>. 随着研究技术的蓬勃发展和材料制备方法的不断改进, 特别是先进表征技术和理论计算方法的应用, 各种新型非晶态合金催化剂不断被开发出来<sup>[26,27]</sup>.

非晶态合金作为新型高效催化剂, 在能源储存和转换领域中具有广泛的应用前景. 与晶态材料相比, 非晶态合金具有如下优势: (1) 非晶态合金催化剂可以在很宽的范围内调整其成分结构, 有利于电子结构的有效调节, 从而获得合适的催化活性中心. (2) 非晶态合金催化剂具有各向同性, 不存在晶界、堆垛层错和偏析等缺陷, 且活性位点均匀. 由于腐蚀往往从晶界开始, 因此非晶态合金催化剂相较于晶态催化剂具有优异的抗腐蚀性能. (3) 非晶态合金的制备方法灵

活且多样, 可根据需求选择制备方式, 从而降低生产成本. (4) 非晶态合金具有较高的表面能及大量不饱和和位点. 表面金属位点在大多数情况下充满悬空键, 使一些化学反应物及中间产物能够适当地吸附在特定位点上, 并在适当的条件下发生反应. (5) 非晶态合金具有亚稳态结构, 在极端物理或化学条件下易发生表面重构, 从惰性物种转变为活性物种. 因此, 非晶态合金催化剂独特的结构优势使其成为一种具有重大应用前景的催化剂材料.

## 3 非晶态合金催化剂的应用

为了实现碳中和和碳达峰的发展目标, 减少传统化石能源的使用是关键. 由于催化反应既能生产又能储存可持续的清洁能源, 所以开发高效催化剂用于能源催化反应是一个行之有效的途径<sup>[28,29]</sup>. 尽管不同催化反应过程产生的可持续能源依赖不同的反应机理, 但其实现及最终商业化必须依赖于高性能催化剂的开发. 非晶态合金作为催化剂具有天然的优势, 在催化领域, 如还原反应催化(包括析氢反应(HER)和氧还原反应(ORR)等)、氧化反应催化(包括析氧反应(OER)、醇氧化反应(AOR)和尿素氧化反应(UOR)等)和污水处理等方面具有巨大的应用潜力.

### 3.1 还原反应

#### 3.1.1 析氢反应(HER)

氢能是一种来源丰富、绿色低碳和应用广泛的二次能源, 正逐步成为全球能源转型发展的重要载体之一<sup>[30]</sup>, 但氢能的发展仍面临诸多问题和挑战. 目前, 主要是通过化石能源和工业副产制氢等方法制氢, 而采用可再生能源制氢的规模仍然较小, 并且用可再生能源制造的氢气才是我们所需要的“绿氢”<sup>[31]</sup>. 在现有的

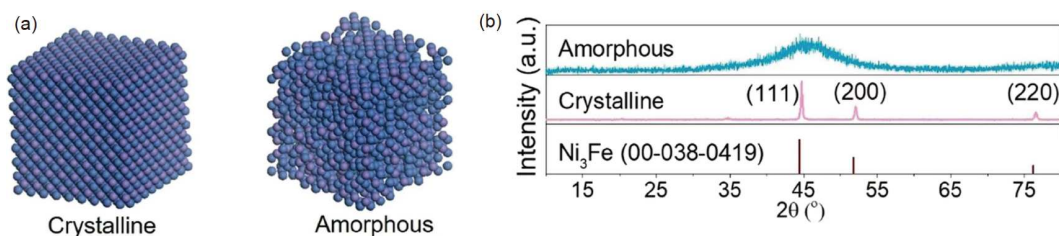


图 2 (网络版彩图)  $\text{Ni}_3\text{Fe}$ 晶体和 $\text{Ni}_3\text{Fe}$ 非晶态合金的原子模型(a)和XRD图谱(b)<sup>[24]</sup>

Figure 2 (Color online) Atomic model (a) and XRD patterns (b) of crystalline and amorphous  $\text{Ni}_3\text{Fe}$  alloys [24].

制氢技术中, 电解水制氢是制备“绿氢”最为广泛使用且行之有效的方法<sup>[32]</sup>. 在传统的电解槽中, 反应是在适当的电解液中进行的, 通常使用硫酸( $\text{H}_2\text{SO}_4$ )和氢氧化钾( $\text{KOH}$ )作为电解液, 分别提供酸性和碱性条件. 析氢反应(HER)作为电解水过程中至关重要的半反应, 在可持续能源转换和储存领域发挥着举足轻重的作用<sup>[33]</sup>. 该反应涉及两电子转移过程, 形成中间氢( $\text{H}^*$ ), 并且受电解液pH值的影响较大<sup>[34]</sup>.

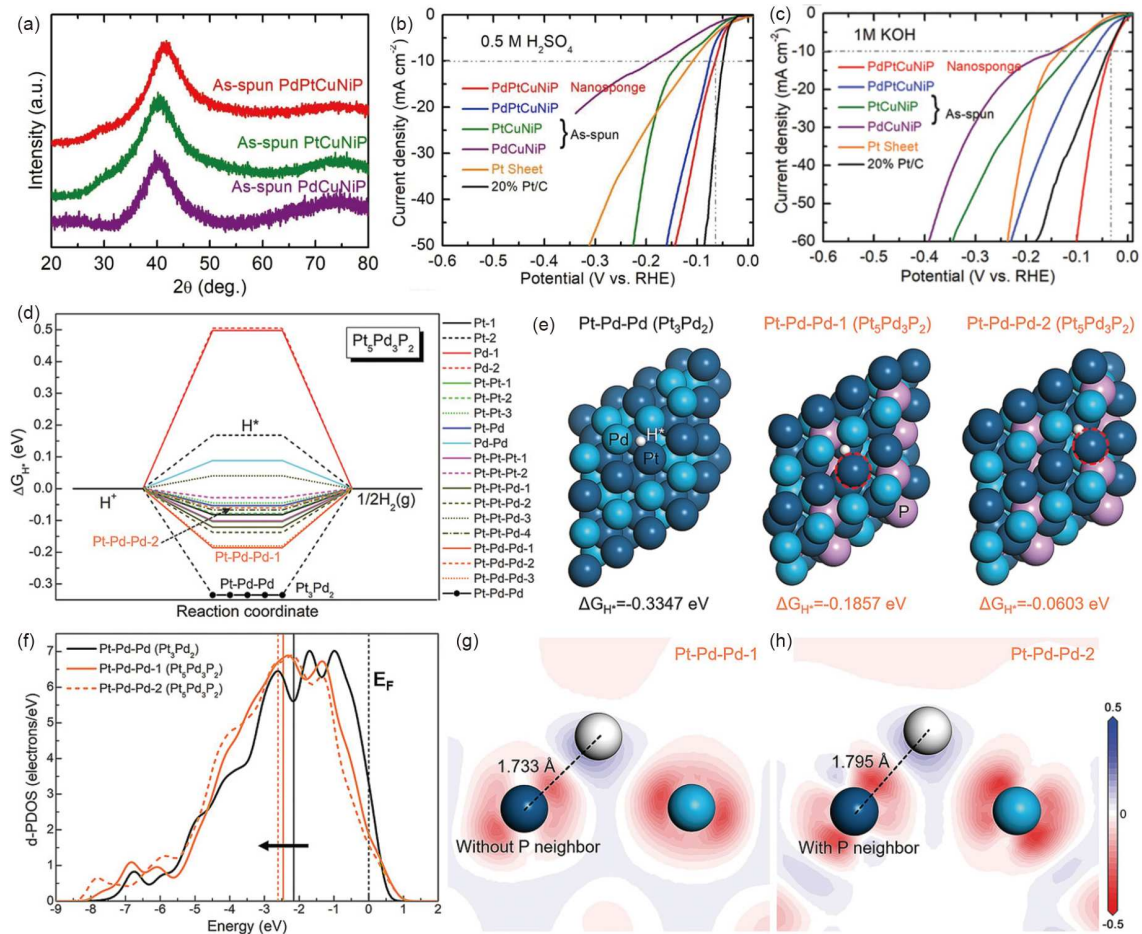
HER的发生需要引入能够降低活化能、加快反应动力学的催化剂. 在研究的非晶态合金催化剂中, 通过电弧熔炼和熔融甩带技术制备的 $\text{Fe}_{40}\text{Co}_{40}\text{P}_{13}\text{C}_7$ <sup>[35]</sup>,  $\text{Pd}_{40}\text{Cu}_{30}\text{Ni}_{10}\text{P}_{20}$ <sup>[36]</sup>和 $\text{Ir}_{25}\text{Ni}_{33}\text{Ta}_{42}$ <sup>[37]</sup>等非晶态合金条带可以作为HER催化剂. 对于传统的电极而言, 活性位点位于电极外表面, 几何面积约等于电化学活性面积(ECSA). 因此, 对于一些纳米材料或3D材料电极, 尤其是一些多孔电极, 其比表面积很大, 会大幅度地增加ECSA, 提升电催化性能<sup>[38]</sup>. 由于非晶条带的表面常常比较光滑, 因此增加其比表面积和反应接触位点从而改善电催化活性是至关重要的. 2021年, Jia等人<sup>[39]</sup>设计了PdPtCuNiP高熵非晶态合金条带(图3(a)), 脱合金后直接用作HER电极, 无论是在碱性还是酸性条件下均显示出优异的HER活性(图3(b)和(c)). 电流密度为 $10 \text{ mA cm}^{-2}$ 时, 在 $1.0 \text{ mol L}^{-1} \text{ KOH}$ 和 $0.5 \text{ mol L}^{-1} \text{ H}_2\text{SO}_4$ 溶液中的过电位( $\eta$ )分别为32和62 mV, 其性能与商业催化剂(Pt/C)媲美. 在酸性和碱性电解液中的稳定性分别为90和100 h, 且元素浸出和结构劣化几乎可以忽略不计, 这表明其具有巨大的商业潜力. 密度泛函理论(DFT)计算和实验表明(图3(d)–(g)), 在脱合金过程中生成的纳米晶具有轻微的晶格畸变, 导致d带中心( $E_d$ )向费米能级( $E_F$ )偏移较大. 这是由Pt-Pd亚晶格中的P原子间隙固溶引起的, 这种固溶现象改善了Pt周围的电子结构, 优化了氢中间体的吸附/脱附, 从而提升

了合金的HER性能. 2022年, Tian等人<sup>[40]</sup>对非晶 $\text{Ti}_{37}\text{Cu}_{60}\text{Ru}_3$ 合金进行脱合金处理, 制备了一种独立的纳米结构HER催化剂, 研究了在TiCu合金中进行脱合金和添加Ru对微观结构在碱性条件下HER性能的影响. 在 $\text{Ti}_{40}\text{Cu}_{60}$ 中添加3 at.%的Ru会降低过电位, 当电流密度达到 $10 \text{ mA cm}^{-2}$ 时, 脱合金样品的过电位和Tafel斜率分别为35 mV和 $34 \text{ mV dec}^{-1}$ . 电催化性能的改善归因于纳米结构的形成和催化剂电子结构的改变. DFT计算结果表明, Ru降低了电解水的吉布斯自由能. Chu等人<sup>[36]</sup>通过高压扭转(HPT)处理的 $\text{Pd}_{40}\text{Cu}_{30}\text{Ni}_{10}\text{P}_{20}$ 非晶态合金, 无论在酸性还是碱性电解液中都表现出优异的HER性能, 而且不会引起明显的结构变化. 严重的塑性变形显著增加了非晶基体中流动单元的密度, 同时也增加了非晶态合金条带的褶皱, 进而增大了其ECSA. 经HPT处理的非晶态合金在 $0.5 \text{ mol L}^{-1} \text{ H}_2\text{SO}_4$ 和 $1 \text{ mol L}^{-1} \text{ KOH}$ 的电解液中, 电流密度达到 $10 \text{ mA cm}^{-2}$ 时的过电位分别为76和209 mV, 低于相同条件下熔融甩带的非晶态合金的179和379 mV. 表1<sup>[41–63]</sup>是近几年部分非晶态合金催化剂用于HER的汇总.

### 3.1.2 氧还原反应(ORR)

在过去的几十年中, 阴极氧还原反应(ORR)产生过氧化氢( $2\text{e}^- \text{ H}_2\text{O}_2$ )引起了人们的极大兴趣, 而在电池能量转换过程中也会涉及四电子氧还原反应( $4\text{e}^- \text{ ORR}$ )<sup>[64]</sup>. ORR的反应过程复杂, 包括多个反应路径和中间产物. 反应路径可以简单地分为四电子路径和两电子路径, 反应路径与电解液的酸碱性有关<sup>[65]</sup>. 当 $\text{O}_2$ 分子吸附在反应活性位点时直接经历 $2\text{e}^- \text{ ORR}$ 过程, 生成的产物为 $\text{H}_2\text{O}_2$ . 然而, 在碱性条件下的ORR途径更倾向于 $4\text{e}^-$ 的还原过程, 最后转化成 $\text{H}_2\text{O}$ . 由于 $4\text{e}^- \text{ ORR}$ 途径的输出电压和能量转换效率高于 $2\text{e}^- \text{ ORR}$ 途





**图 3** (网络版彩图) (a) XRD图谱; (b), (c) 在  $0.5 \text{ mol L}^{-1} \text{ H}_2\text{SO}_4$  (b) 和  $1 \text{ mol L}^{-1} \text{ KOH}$  (c) 溶液中的线性扫描伏安(LSV)极化曲线; (d)  $\text{Pt}_5\text{Pd}_3\text{P}_2$  的吉布斯自由能曲线; (e)  $\text{Pt}_3\text{Pd}_2$  和  $\text{Pt}_5\text{Pd}_3\text{P}_2$  的 Pt-Pd-Pd 位点吸附  $\text{H}^*$  的局部环境及相应的吉布斯自由能 ( $\Delta G_{\text{H}^*}$ ) 值; (f) Pt-Pd-Pd 位点在不同环境下的 d-PDOS 和相应的 d 带中心 ( $E_d$ ); (g), (h) 在无 P (g) 和有 P (h) 的  $\text{Pt}_5\text{Pd}_3\text{P}_2$  表面上,  $\text{H}^*$  吸附在 Pt-Pd-Pd 第一邻位配位点后的电荷密度差分的 DFT 结果<sup>[39]</sup>

**Figure 3** (Color online) (a) XRD patterns; (b), (c) polarization curves of LSV in  $0.5 \text{ mol L}^{-1} \text{ H}_2\text{SO}_4$  (b) and  $1 \text{ mol L}^{-1} \text{ KOH}$  (c) solutions; (d) Gibbs free energy curve of  $\text{Pt}_5\text{Pd}_3\text{P}_2$  surface; (e) the local environment of  $\text{H}^*$  adsorbed at Pt-Pd-Pd sites of  $\text{Pt}_3\text{Pd}_2$  and  $\text{Pt}_5\text{Pd}_3\text{P}_2$  and the corresponding Gibbs free energy ( $\Delta G_{\text{H}^*}$ ) values; (f) the d-PDOS results and the corresponding d-band center ( $E_d$ ) for the Pt-Pd-Pd sites with different neighboring environments; (g), (h) DFT results of electron density differences after  $\text{H}^*$  adsorption on Pt-Pd-Pd sites at the  $\text{Pt}_5\text{Pd}_3\text{P}_2$  surface without (g) and with (h) first neighboring coordination of P [39].

径, 因此  $4\text{e}^-$  ORR 过程得到了广泛的认可. 由于 ORR 的动力学过程缓慢, 通常需要更高的过电位才能获得实际电流密度<sup>[66]</sup>, 导致实际电化学能量转换效率较低. 为了提高反应速率, 需要设计高效的催化剂, 以降低中间体之间过渡态的最大势垒.

在探索  $2\text{e}^-$  ORR 催化剂时, 非晶态合金催化剂受到了研究者的关注. 2022 年, Wu 等人<sup>[67]</sup> 研究发现在  $0.2\text{--}0.6 \text{ V/RHE}$  (可逆氢电极) 的电位范围内,  $\text{NiB}_2$  非晶态合金催化剂对  $\text{H}_2\text{O}_2$  的选择性超过 93%, 在  $0.4 \text{ V/RHE}$  可达 99%, 可以在 12 h 内保持优异的活性, 衰减可以忽

略不计(图 4(a)–(c)), 性能超过了之前报道的先进催化剂. 这种非晶态合金催化剂同时具有低成本、高活性、高选择性和稳定性的优点, 有效解决了  $2\text{e}^-$  ORR 稳定性不足的问题.

除此之外, 在探索  $4\text{e}^-$  ORR 催化剂时, 研究者们也发现了非晶态合金催化剂的优越性. 2023 年, Fu 等人<sup>[68]</sup> 通过新型激光蒸发惰性气体冷凝法, 合成了一种具有球形形态的、新颖的  $\text{Pd}_{40}\text{Ni}_{40}\text{P}_{20}$  拓扑无序金属玻璃纳米颗粒(MGNP). 通过结构分析揭示了 Pd-Ni-P MGNP 团簇连接成中程序(MRO)时从两个原子模式转

表 1 非晶态合金的HER催化性能

Table 1 HER catalytic performance of amorphous alloys

| 催化剂                                                                                  | 电解液                                                    | 过电位                   | 稳定性测试                          | 文献   |
|--------------------------------------------------------------------------------------|--------------------------------------------------------|-----------------------|--------------------------------|------|
| RhRuPtPdIr                                                                           | 0.5 mol L <sup>-1</sup> H <sub>2</sub> SO <sub>4</sub> | $\eta_{10} = 13$ mV   | 12 h@-100 mA cm <sup>-2</sup>  | [41] |
|                                                                                      | 1.0 mol L <sup>-1</sup> PBS                            | $\eta_{10} = 77$ mV   |                                |      |
|                                                                                      | 1.0 mol L <sup>-1</sup> KOH                            | $\eta_{10} = 65$ mV   |                                |      |
| Fe <sub>67</sub> Co <sub>10</sub> Ni <sub>10</sub> Zr <sub>10</sub> Pt <sub>3</sub>  | 1.0 mol L <sup>-1</sup> KOH                            | $\eta_{10} = 19$ mV   | 250 h@-500 mA cm <sup>-2</sup> | [42] |
| NiZrPt                                                                               | 1.0 mol L <sup>-1</sup> KOH                            | $\eta_{10} = 15$ mV   | 100 h@-10 mA cm <sup>-2</sup>  | [43] |
| Cu <sub>50</sub> W <sub>50</sub>                                                     | 1.0 mol L <sup>-1</sup> KOH                            | $\eta_{10} = 65$ mV   | 200 h@-100 mA cm <sup>-2</sup> | [44] |
| Fe <sub>88.46</sub> P <sub>9.42</sub>                                                | 1.0 mol L <sup>-1</sup> KOH                            | $\eta_{10} = 436$ mV  | 207 h@-10 mA cm <sup>-2</sup>  | [45] |
| Co-P-B                                                                               | 1.0 mol L <sup>-1</sup> KOH                            | $\eta_{10} = 270$ mV  | 10000 CV                       | [46] |
| CoP                                                                                  | 1.0 mol L <sup>-1</sup> KOH                            | $\eta_{10} = 63$ mV   | 2000 CV                        | [47] |
| a-CoPSe                                                                              | 1.0 mol L <sup>-1</sup> KOH                            | $\eta_{100} = 212$ mV | 1000 CV                        | [48] |
| FeCoCrMoCBY                                                                          | 0.5 mol L <sup>-1</sup> H <sub>2</sub> SO <sub>4</sub> | $\eta_{100} = 178$ mV | 120 h@-50 mA cm <sup>-2</sup>  | [49] |
| PdPtCuNiP                                                                            | 0.5 mol L <sup>-1</sup> H <sub>2</sub> SO <sub>4</sub> | $\eta_{10} = 35.4$ mV | 6 h@-1.25 V/RHE                | [50] |
| Pt <sub>25</sub> Pd <sub>25</sub> Ni <sub>25</sub> P <sub>25</sub>                   | 1.0 mol L <sup>-1</sup> KOH                            | $\eta_{10} = 19.8$ mV | 20 h@-60 mA cm <sup>-2</sup>   | [51] |
| (FeCoNiB <sub>0.75</sub> ) <sub>97</sub> Pt <sub>3</sub>                             | 1.0 mol L <sup>-1</sup> KOH                            | $\eta_{10} = 27$ mV   | 48 h@-20 mA cm <sup>-2</sup>   | [52] |
| Fe <sub>73.5</sub> Si <sub>13.5</sub> B <sub>9</sub> Cu <sub>1</sub> Nb <sub>3</sub> | 1.0 mol L <sup>-1</sup> KOH                            | $\eta_{10} = 174$ mV  | 40 h@CV                        | [53] |
| FeCoNiAlP                                                                            | 1.0 mol L <sup>-1</sup> KOH                            | $\eta_{10} = 134$ mV  | 24 h@-1.34 V/RHE               | [54] |
| FeNiCoMoP                                                                            | 1.0 mol L <sup>-1</sup> KOH                            | $\eta_{10} = 146$ mV  | 24 h@-10 mA cm <sup>-2</sup>   | [55] |
| FeMoPC                                                                               | 0.5 mol L <sup>-1</sup> H <sub>2</sub> SO <sub>4</sub> | $\eta_{10} = 96$ mV   | 16 h@-10 mA cm <sup>-2</sup>   | [56] |
| Cu <sub>60</sub> Ti <sub>37</sub> Mo <sub>3</sub>                                    | 1.0 mol L <sup>-1</sup> KOH                            | $\eta_{10} = 220$ mV  | 20 h@220 mV                    | [57] |
| Ni <sub>69</sub> P <sub>31</sub>                                                     | 0.5 mol L <sup>-1</sup> H <sub>2</sub> SO <sub>4</sub> | $\eta_{10} = 275$ mV  | 1600 CV                        | [58] |
| NiMo                                                                                 | KOH (PH = 10)                                          | $\eta_{10} = 63.9$ mV | 100 h@-10 mA cm <sup>-2</sup>  | [59] |
| Ni-Ce-Pr-Ho                                                                          | 1.0 mol L <sup>-1</sup> KOH                            | $\eta_{10} = 78$ mV   | 24 h@-10 mA cm <sup>-2</sup>   | [60] |
| AlMnYNiCoAu                                                                          | 1.0 mol L <sup>-1</sup> KOH                            | $\eta_{10} = 124$ mV  | 18 h@-10 mA cm <sup>-2</sup>   | [61] |
| Mg <sub>80</sub> Ni <sub>20</sub>                                                    | 1.0 mol L <sup>-1</sup> KOH                            | $\eta_{10} = 33.1$ mV | 100 h@-20 mA cm <sup>-2</sup>  | [62] |
| D-NiNbIrPt                                                                           | 1.0 mol L <sup>-1</sup> KOH                            | $\eta_{10} = 19$ mV   | 1000 h@-0.5 A cm <sup>-2</sup> | [63] |

变为三个原子模式, 稳定了MGNP的非晶态结构, 并防止了结晶引起的性能下降. 这种MRO结构变化不是由ORR过程中的部分表面氧化衍生而来的, 因为氧化往往会降低电催化剂的ORR性能, 而MRO结构演变有利于MGNPs在ORR中的稳定性. Pd-Ni-P MGNP在氧饱和的0.1 mol L<sup>-1</sup> KOH电解液中表现出优异的电催化活性和稳定性. 在1600 r min<sup>-1</sup>的起始电位和半波电位( $E_{1/2}$ )分别为0.96和0.84 V/RHE, 且经过1000次循环伏安测试(CV)后的极化曲线的起始电位几乎没有变化, 半波电位仅降低了10 mV, 这表明Pd-Ni-P MGNPs具有很高的稳定性(图4(d)-(f)).

## 3.2 氧化反应

### 3.2.1 析氧反应(OER)

电解水由两个半反应组成, 分别是阳极的析氧反应(OER)和阴极的析氢反应(HER)<sup>[69]</sup>. 然而, 由于OER反

应涉及四电子-质子耦合反应过程, 动力学过程非常缓慢<sup>[70]</sup>. 因此, 在实际反应中, 实现电解水所施加的电极电位要远高于理论电解水动力学电位1.23 V/RHE<sup>[71]</sup>. 即使在使用催化剂的情况下, 也难以将实际电极电位降到1.23 V/RHE, 这导致制氢的能耗和成本过高<sup>[72]</sup>. 因此, OER是电解水技术发展的一个主要瓶颈, 需要开发高效的催化剂来克服OER较高的过电位. 另外, OER也受电解液pH值的影响较大<sup>[73]</sup>, 其反应步骤涉及不同的反应物、产物以及各种反应中间体的吸附/脱附, 包括O\*, HO\*和HOO\*等中间体, 也导致了OER过程的复杂性.

过渡金属Ni/Co/Fe基等非晶态合金体系同时具备廉价、3d轨道未满以及短程有序的特点, 从而使其在电解水领域成为研究热点. 2017年, Tan等人<sup>[74]</sup>探索了Ni-Fe-P非晶条带的OER性能, 原始非晶条带的OER过电位约为320 mV, 催化性能可与商业催化剂IrO<sub>2</sub>媲美

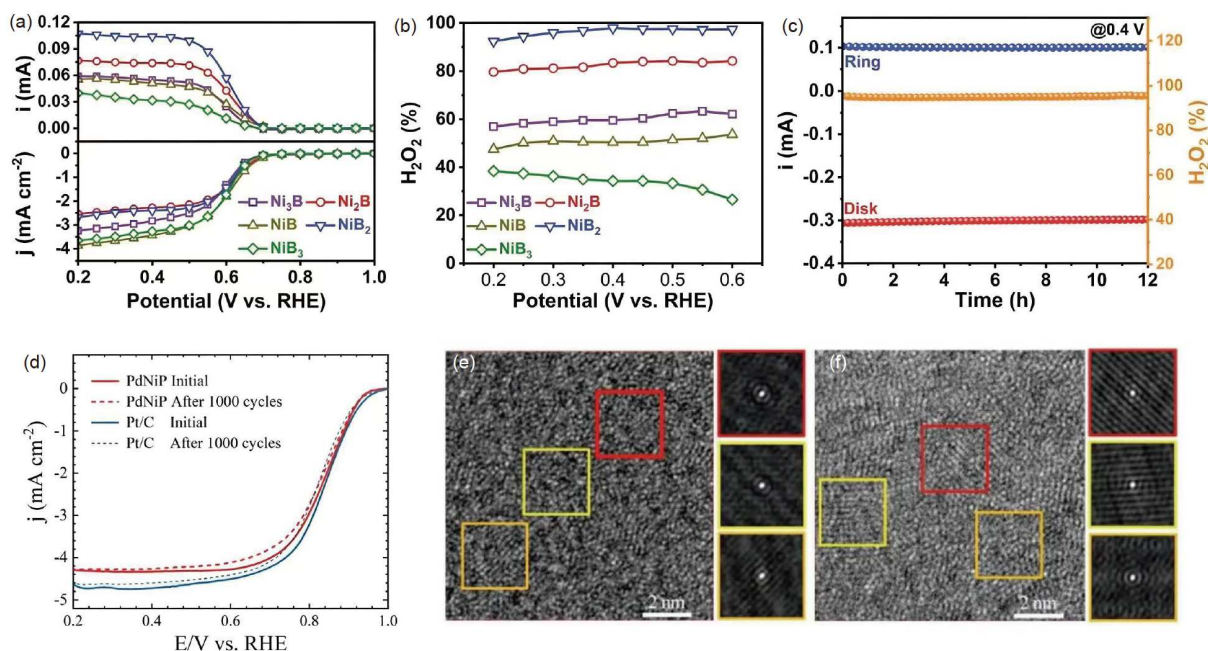


图 4 (网络版彩图) (a) Ni-B样品的LSV曲线; (b) 根据LSV曲线计算的相应H<sub>2</sub>O<sub>2</sub> (%); (c) 在0.4 V/RHE条件下, NiB<sub>2</sub>在氧饱和0.1 mol L<sup>-1</sup> KOH条件下的计时电流法测试(*i*<sub>disk</sub>为盘电流密度, *i*<sub>ring</sub>为环电流密度)<sup>[67]</sup>; (d) Pd-Ni-P/C和Pt/C在氧饱和0.1 mol L<sup>-1</sup> KOH中的LSV曲线(1600 r min<sup>-1</sup>); (e), (f) Pd-Ni-P MGNPs经历1000 CV循环前(e)和1000 CV循环后(f)的HRTEM图像<sup>[68]</sup>

**Figure 4** (Color online) (a) LSV curves of the Ni-B samples; (b) the calculated H<sub>2</sub>O<sub>2</sub> (%) of the corresponding LSV curves; (c) chronoamperometry of NiB<sub>2</sub> at 0.4 V/RHE in O<sub>2</sub>-saturated 0.1 mol L<sup>-1</sup> KOH (where the disk current density (*i*<sub>disk</sub>) together with the ring currents (*i*<sub>ring</sub>) [67]; (d) LSV curves for Pd-Ni-P/C and Pt/C in O<sub>2</sub>-saturated 0.1 mol L<sup>-1</sup> KOH (1600 r min<sup>-1</sup>); (e), (f) HRTEM images for the Pd-Ni-P MGNPs before (e) and after (f) 1000 CV cycles [68].

( $\eta_{10} \approx 320$  mV), 通过表面处理后过电位降低至 255 mV. Hu 等人<sup>[75]</sup>通过对 Ni-Fe-P 非晶条带中的元素比例进行调控以及表面处理, 进一步提高了 Ni-Fe-P 非晶条带的 OER 性能, 过电位降低至 219 mV, OER 催化性能已远远优于商业催化剂. 2022 年, Li 等人<sup>[76]</sup>通过控制非晶形成金属液体的凝固行为, 在界面处获得了丰富的高能原子台阶. 通过调整化学成分和冷却速率, 在 Fe-Ni-B 金属玻璃(MG)基体中原位形成 FeNi<sub>3</sub> 纳米晶, 从而产生有序/无序的锯齿状原子台阶界面(图 5(b)–(d)). 最优的 FeNi<sub>3</sub> 纳米晶/MG 复合材料在 10 mA cm<sup>-2</sup> 的电流密度下的过电位和 Tafel 斜率分别为 214 mV 和 32.4 mV dec<sup>-1</sup>, 并在碱性电解液中具有良好的稳定性(120 h) (图 5(e)–(g)), 优于大多数先进的催化剂. 该方法基于对非晶形成液体中纳米晶的成核和生长速度的控制, 借助过冷状态时的动力学阻挫效应, 可以获得高度阶梯式的界面结构.

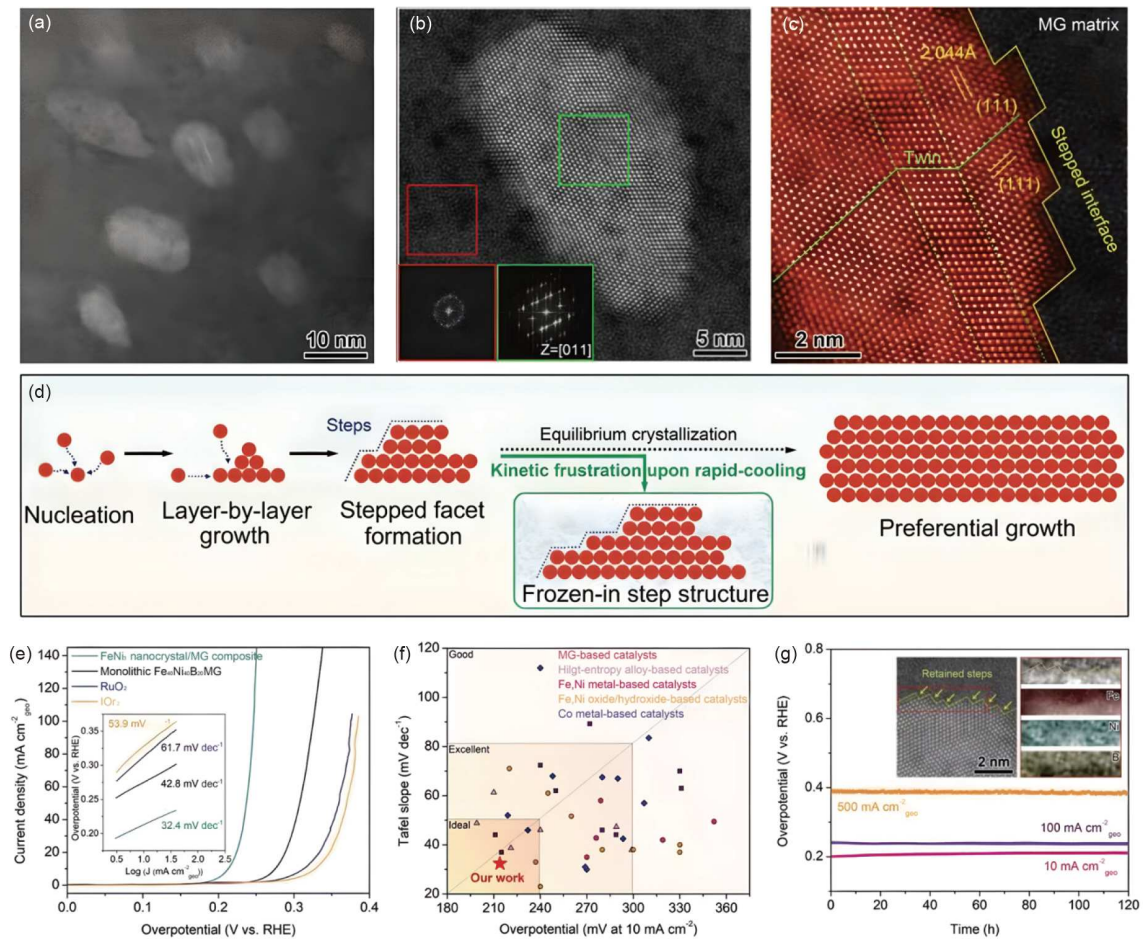
上述研究可以看出, 纳米晶/非晶复合材料可以作为一种有效的策略提升电催化性能. 纳米晶/非晶复合

材料结合了丰富的催化位点和良好的导电性这两个关键因素, 是实现高性能催化剂的候选材料. 2022 年, Zhang 等人<sup>[77]</sup>通过 NaBH<sub>4</sub> 水解和高温磷化(NaH<sub>2</sub>PO<sub>2</sub>) 工艺, 成功制备了由 Fe<sub>3</sub>P<sub>0.37</sub>B<sub>0.63</sub> 合金纳米颗粒修饰的非晶态 Ni<sub>2</sub>P 和 Fe<sub>2</sub>P 纳米片组成的 FePB/NiFeP 纳米晶/非晶复合催化剂. FePB/NiFeP 纳米晶/非晶复合催化剂表现出优异的 OER 性能和稳定性, 当电流密度达到 10 mA cm<sup>-2</sup> 时, 过电位仅为 182 mV, Tafel 斜率为 43.9 mV dec<sup>-1</sup>, 优于大多数过渡金属基 OER 电催化剂. 除此之外, Zhang 等人<sup>[78–81]</sup>发现, 晶体材料, 尤其是高熵合金(HEA), 在电催化过程中极容易发生表面重构, 生成大量金属氧化物和局域非晶结构, 表现出优异的 OER 性能. 这些研究为其他先进合金催化剂的设计提供了思路. 表 2<sup>[82–102]</sup>是近几年部分非晶态合金催化剂用于 OER 的汇总.

### 3.2.2 醇氧化反应(AOR)

OER 是电解水整体能量转换效率的制约因素, 除





**图 5** (网络版彩图) (a) 原位析出FeNi<sub>3</sub>纳米晶的Fe<sub>40</sub>Ni<sub>40</sub>B<sub>20</sub> MG复合材料HRTEM图像; (b) FeNi<sub>3</sub>纳米晶的HAADF-STEM图像, 插图显示了所选区域的FFT模式; (c) FeNi<sub>3</sub>纳米晶与MG基体间阶梯界面的原子结构; (d) 阶梯界面结构在快速凝固过程中的形成过程示意图; (e) OER极化曲线; (f) FeNi<sub>3</sub>纳米晶/MG复合材料与最近报道的各种过渡金属基电催化剂在碱性电解液中的OER活性比较; (g) 计时电位曲线<sup>[76]</sup>

**Figure 5** (Color online) (a) HRTEM image of the as-spun Fe<sub>40</sub>Ni<sub>40</sub>B<sub>20</sub> MG composite with *in situ* precipitated FeNi<sub>3</sub> nanocrystals; (b) HAADF-STEM image of the FeNi<sub>3</sub> nanocrystal, the insets show the FFT patterns of the selected areas; (c) atomic structure of the stepped interface between the twinned FeNi<sub>3</sub> nanocrystal and MG matrix; (d) schematic illustration of the formation process of the stepped interface architecture during rapid solidification; (e) OER polarization curves; (f) comparison of the OER activity of the FeNi<sub>3</sub> nanocrystal/MG composite with various recently reported transition metal-based electrocatalysts in alkaline; (g) chrono-potentiometric curves <sup>[76]</sup>.

了开发低成本、高效率的OER催化剂外, 利用热力学反应势垒更低的醇氧化反应(AOR)来替代OER被认为是解决阳极氧化瓶颈的一种策略<sup>[103]</sup>. 这种替代可以在阳极产生比O<sub>2</sub>更有价值的化学物质. 甲醇氧化反应(MOR)和乙醇氧化反应(EOR)是替代OER的有效阳极反应, 因为它们需要的电位很低<sup>[104]</sup>. 此外, MOR避免了H<sub>2</sub>与O<sub>2</sub>的混合并防止制备过程中发生爆炸的风险, 也无需进行气体分离即可生产纯氢气. 除此之外, 直接醇燃料电池(DAFC)也可作为解决全球环境问题和能源问题的一条可行途径. 然而, 由于阳极反应(AOR)动

力学缓慢, 也阻碍了DAFC的广泛应用<sup>[105]</sup>. 目前的晶态催化剂通常存在催化效率低、CO中毒严重和活性衰减快等问题, 极大地限制了其实际应用<sup>[106]</sup>. 因此, 开发高活性和稳定性的非晶态合金催化剂用于提高AOR氧化反应效率是一个极具前景的策略.

2018年, Xu等人<sup>[19]</sup>通过电化学脱合金工艺实现选择性溶解具有低“分离极限”的Au<sub>55</sub>Cu<sub>25</sub>Si<sub>20</sub>金属玻璃条带中的一种元素, 形成三维“圆锥形突起”纳米多孔结构. 一方面, 这种3D多孔结构提供了高密度的本征催化位点, 因为“锥形突起”内部在凹凸区域之间具

表 2 非晶态合金的OER催化性能

Table 2 OER catalytic performance of amorphous alloys

| 催化剂                                                                                                                       | 电解液                               | 过电位                                          | 稳定性测试                         | 文献    |
|---------------------------------------------------------------------------------------------------------------------------|-----------------------------------|----------------------------------------------|-------------------------------|-------|
| FeCoNiMoVO                                                                                                                | 1.0 mol L <sup>-1</sup> KOH<br>海水 | $\eta_{10} = 216$ mV<br>$\eta_{10} = 236$ mV | 100 h@1 A cm <sup>-2</sup>    | [82]  |
| FeCoMoPB                                                                                                                  | 1.0 mol L <sup>-1</sup> KOH       | $\eta_{10} = 239$ mV                         | 48 h@10 mA cm <sup>-2</sup>   | [83]  |
| Ni <sub>28</sub> Fe <sub>42</sub> Mn <sub>30</sub>                                                                        | 1.0 mol L <sup>-1</sup> KOH       | $\eta_{100} = 282$ mV                        | 100 h@100 mA cm <sup>-2</sup> | [84]  |
| Ni <sub>40</sub> Fe <sub>40</sub> B <sub>20</sub>                                                                         | 1.0 mol L <sup>-1</sup> KOH       | $\eta_{10} = 319$ mV                         | 24 h@10 mA cm <sup>-2</sup>   | [85]  |
| Fe <sub>50</sub> Ni <sub>27</sub> Nb <sub>3</sub> P <sub>13</sub> C <sub>7</sub>                                          | 6.0 mol L <sup>-1</sup> KOH       | $\eta_{10} = 248$ mV                         | 18 h@10 mA cm <sup>-2</sup>   | [86]  |
| FeCoNiCrMo <sub>x</sub>                                                                                                   | 1.0 mol L <sup>-1</sup> KOH       | $\eta_{100} = 294.5$ mV                      | 160 h@100 mA cm <sup>-2</sup> | [87]  |
| FeCoNiMoPB                                                                                                                | 1.0 mol L <sup>-1</sup> KOH       | $\eta_{10} = 281$ mV                         | 107 h@10 mA cm <sup>-2</sup>  | [88]  |
| Fe <sub>40</sub> Co <sub>40</sub> B <sub>20</sub>                                                                         | 1.0 mol L <sup>-1</sup> KOH       | $\eta_{10} = 315$ mV                         | 24 h@10 mA cm <sup>-2</sup>   | [89]  |
| Ni <sub>50</sub> Fe <sub>25</sub> B <sub>15</sub> Si <sub>7</sub> P <sub>3</sub>                                          | 1.0 mol L <sup>-1</sup> KOH       | $\eta_{10} = 235$ mV                         | 80 h@10 mA cm <sup>-2</sup>   | [90]  |
| Co-W-B                                                                                                                    | 1.0 mol L <sup>-1</sup> KOH       | $\eta_{10} = 292$ mV                         | 10 h@300 mV                   | [91]  |
| FeNiCo-ANs                                                                                                                | 1.0 mol L <sup>-1</sup> KOH       | $\eta_{10} = 274$ mV                         | 10 h@30 mA cm <sup>-2</sup>   | [92]  |
| Fe <sub>78</sub> Si <sub>9</sub> B <sub>13</sub>                                                                          | 1.0 mol L <sup>-1</sup> KOH       | $\eta_{10} = 240$ mV                         | 48 h@10 mA cm <sup>-2</sup>   | [93]  |
| Ni <sub>40</sub> Fe <sub>40</sub> B <sub>20</sub>                                                                         | 1.0 mol L <sup>-1</sup> KOH       | $\eta_{10} = 249$ mV                         | 100 h@100 mA cm <sup>-2</sup> | [94]  |
| Fe <sub>40</sub> Ni <sub>20</sub> Co <sub>20</sub> P <sub>15</sub> C <sub>5</sub>                                         | 1.0 mol L <sup>-1</sup> KOH       | $\eta_{10} = 236$ mV                         | 20 h@330 mV                   | [95]  |
| NiFeCoP                                                                                                                   | 1.0 mol L <sup>-1</sup> KOH       | $\eta_{10} = 245$ mV                         | 20 h@10 mA cm <sup>-2</sup>   | [96]  |
| (FeCoNi) <sub>80</sub> P <sub>14</sub> B <sub>6</sub>                                                                     | 1.0 mol L <sup>-1</sup> HCl       | $\eta_{10} = 229$ mV                         | 25 h@350 mA cm <sup>-2</sup>  | [97]  |
| FeNiCoP                                                                                                                   | 1.0 mol L <sup>-1</sup> NaOH      | $\eta_{10} = 281$ mV                         | 20 h@10 mA cm <sup>-2</sup>   | [98]  |
| (Fe <sub>73.5</sub> Si <sub>13.5</sub> B <sub>9</sub> Nb <sub>3</sub> Cu <sub>1</sub> ) <sub>91.5</sub> Ni <sub>8.5</sub> | 1.0 mol L <sup>-1</sup> KOH       | $\eta_{10} = 230$ mV                         | —                             | [99]  |
| (Ni <sub>0.4</sub> Fe <sub>0.4</sub> B <sub>0.2</sub> ) <sub>100-x</sub> Ru <sub>x</sub>                                  | 1.0 mol L <sup>-1</sup> KOH       | $\eta_{10} = 245$ mV                         | 15 h@10 mA cm <sup>-2</sup>   | [100] |
| Ir <sub>25</sub> Ni <sub>33</sub> Ta <sub>42</sub>                                                                        | 1.0 mol L <sup>-1</sup> KOH       | $\eta_{10} = 266$ mV                         | 10 h@10 mA cm <sup>-2</sup>   | [101] |
| Fe <sub>29</sub> Co <sub>27</sub> Ni <sub>23</sub> Si <sub>9</sub> B <sub>12</sub> HEA                                    | 1.0 mol L <sup>-1</sup> KOH       | $\eta_{10} = 230$ mV                         | 50 h@100 mA cm <sup>-2</sup>  | [102] |

有较大的曲率梯度, 并且具有大量的低配位原子位点. 另一方面, 理论和实验工作已经表明, 弹性应变可以增强分子相互作用, 从而减少化学反应的能垒. 因此, 多孔“锥形突起”内部结构和应变效应的相互作用可有效提高电催化能力. 当甲醇浓度增加到2 mol L<sup>-1</sup>时, 甲醇氧化电位峰负向偏移至0.31 V/Ag/AgCl, 最优的MOR活性达到232.5  $\mu\text{A cm}^{-2}$ . 除了MOR行为, Au<sub>55</sub>Cu<sub>25</sub>Si<sub>20</sub>金属玻璃电极还具有更优异的EOR电化学性能. 当乙醇浓度增加到2 mol L<sup>-1</sup>时, EOR的起始电位从-0.05 V/Ag/AgCl负向偏移到-0.18 V/Ag/AgCl, 最大活性从451  $\mu\text{A cm}^{-2}$ 提高到928  $\mu\text{A cm}^{-2}$ . 另外, 2020年, Baksi等人<sup>[107]</sup>也报道了Ni<sub>60</sub>Nb<sub>40</sub>金属玻璃具有较高的MOR性能.

### 3.2.3 尿素氧化反应(UOR)

由于四电子反应的动力学缓慢, 阳极的OER在很大程度上阻碍了制氢效率. 除了开发上述AOR催化剂可以代替OER外, 也可以用热力学势垒较低的其他电催化氧化反应(如尿素/氨/生物质氧化)代替OER, 这也被认为是实现节能制氢的可行方法<sup>[108]</sup>. 通常, 尿素广

泛存在于不同的废水(如人类尿液、工业废水)中<sup>[109]</sup>, 因此尿素氧化反应(UOR)工艺不仅是高效制氢的关键反应<sup>[110]</sup>, 还可以净化各种含尿素废水, 这对经济和环境都具有重要意义. 为了降低UOR能耗, 开发用于UOR的高效催化剂是当务之急.

Pei等人<sup>[20]</sup>证明了电沉积的Ni-P纳米玻璃(NG)由于其异质结构而具有极高的能态, 而催化性能将受益于高能状态. 特别是较高的表面能等效于较高的活性, 该活性来自催化剂表面较多的低配位位点. 而且, 具有异质结构的Ni-P NG是制备独特的蜂窝状纳米孔结构的完美前驱体, 在UOR中表现出优异的催化性能. 具体来说, 优化后的Ni-P NG在电流密度达到10 mA cm<sup>-2</sup>时仅需要1.36 V/RHE的电位, Tafel斜率仅为13 mV dec<sup>-1</sup>, UOR性能远优于其他镍基合金. 除此之外, Ni-P NG在1.0 mol L<sup>-1</sup> KOH溶液中也具有很好的OER性能, 即在电流密度达到10 mA cm<sup>-2</sup>时仅需要1.54 V/RHE的电位(图6(a)-(e)). 2024年, Sohel等人<sup>[111]</sup>报道了Ni<sub>60</sub>Nb<sub>40</sub>纳米玻璃异质界面作为一种有前途的无黏结剂、自支撑电极UOR催化剂. 通过原位生成稳



定的 $\gamma$ -NiOOH活性物质促进了氧化, 在 $1.0 \text{ mol L}^{-1}$  KOH的碱性电解液中,  $\text{Ni}_{60}\text{Nb}_{40}$ 纳米玻璃在施加电位下表面易原位生成 $\gamma$ -NiOOH, 这进一步有效控制了UOR动力学, Tafel斜率低至 $16 \text{ mV dec}^{-1}$ , 并且在 $38 \text{ mA cm}^{-2}$ 的电流密度下可进行长达70 h的长电催化反应, 表明了其优异的稳定性, 这归因于纳米结构的玻璃界面促进了更多 $\gamma$ -NiOOH物种的形成. 表面稳定的 $\text{Ni}_{60}\text{Nb}_{40}$ 纳米玻璃也表现出类似的机制, 独特的纳米结构、玻璃颗粒和界面的存在导致了高活性物种的产生.

### 3.3 非晶态合金催化剂在污水处理领域的应用

纺织工业废水逐渐成为一个严峻的环境问题, 从废水中去除染料在环境工程方面具有巨大的发展潜力<sup>[112]</sup>. 目前, 全球每年生产超过70万吨有机染料, 其中偶氮染料的种类高达10000多种, 约占商业染料总产量的60%–70%<sup>[113]</sup>, 这类偶氮染料通常具有各种颜色. 偶氮染料具有高度耐久性、毒性, 并可在生物体内累积, 对生物体和人类产生较大的威胁<sup>[114]</sup>. 据报道, 只有45%–47%的有机染料可以生物降解并溶解于水, 其余

53%–55%的偶氮染料是有害的<sup>[26]</sup>, 它们的降解已成为一个紧迫的问题. 为了开发有效的技术来降解和净化被染料污染的水体, 人们尝试了各种催化剂来修复染料废水<sup>[115]</sup>. 虽然各种纳米催化剂相继被开发, 但是这些纳米催化剂的循环使用次数极其有限, 其分离难度大<sup>[116]</sup>也限制了它们的实际应用.

2020年, Miao等人<sup>[117]</sup>报道了FeBC非晶条带对酸性橙7 (AO7)具有高效降解能力, 并将其与FePC非晶条带进行了比较(图7(a)–(d)). 使用FeBC非晶条带降解50%的AO7所需的时间仅为使用FePC条带的1/3. 在FeBC非晶条带中, 由于Fe–B键和Fe–C键之间的键合强度差异大, 形成了原电池结构, 这导致FeBC非晶条带的反应活化能低且降解效率高. FeBC非晶条带不仅在酸性条件下具有优异的AO7降解能力, 而且在中性和弱碱性环境中也均具有优异的降解能力. 2022年, Peng等人<sup>[118]</sup>利用沉积过程中的可控表面扩散和抑制晶体粗化过程, 利用具有纳米级相分离的MG薄膜前体制备了致密非晶-晶体(a/c)复合界面的超细a/c FeS–iBNb催化剂. 该超细a/c催化剂表现出优异的循环降解

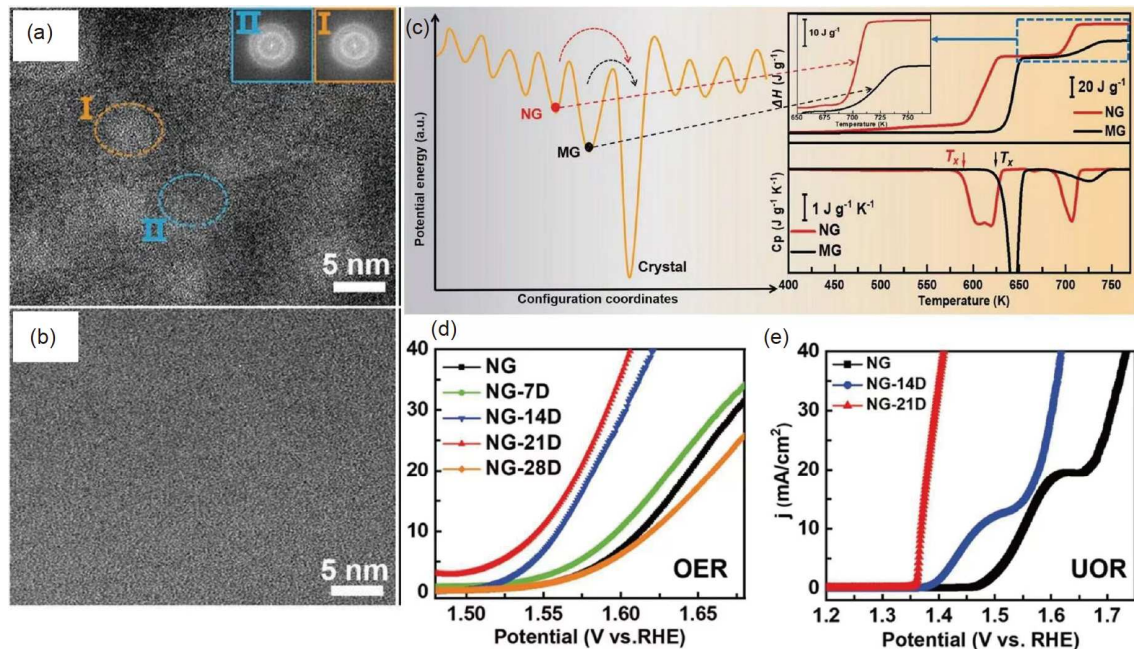
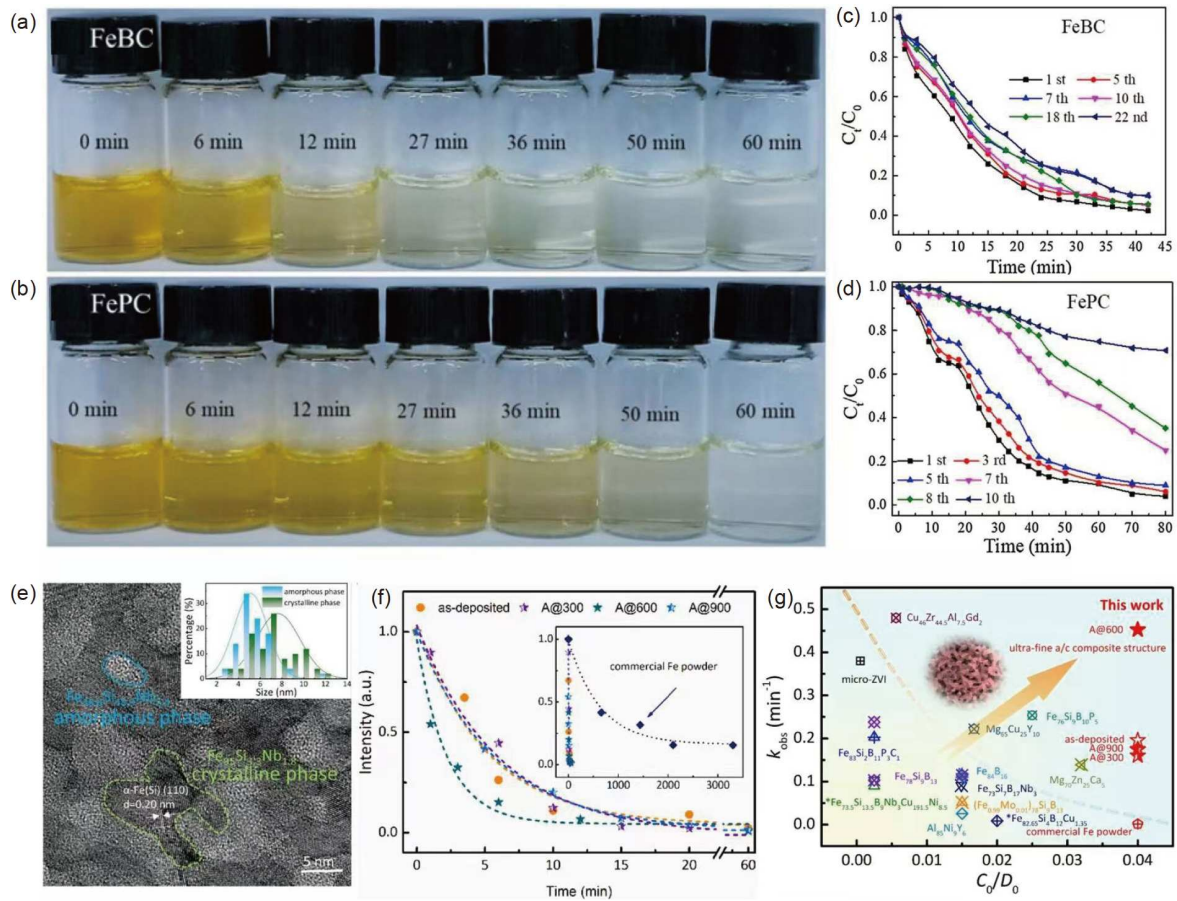


图 6 (网络版彩图) (a), (b) NG (a)和MG (b)的HRTEM图像. (c) 左图是NG和MG的势能分布示意图. 右下方图是加热速率为 $20 \text{ K min}^{-1}$ 时NG和MG的热容曲线. 右上方图是由NG和MG热容曲线积分得到的焓变( $\Delta H$ )曲线, 其中插图是 $\Delta H$ 曲线的放大图像. (d) OER极化曲线. (e) UOR极化曲线<sup>[20]</sup>

**Figure 6** (Color online) (a), (b) HRTEM images of NG (a) and MG (b). (c) The left is a schematic diagram of the potential energy landscape of the NG and MG. Heat capacity curves of the MG and NG are exhibited on the lower right for the heating rate of  $20 \text{ K min}^{-1}$ . Enthalpy change ( $\Delta H$ ) curves obtained by the integration of the heat capacity curves are displayed on the top right, where the insert is the enlarged image of the  $\Delta H$  curves. (d) OER polarization curves. (e) UOR polarization curves<sup>[20]</sup>.



**图 7** (网络版彩图) (a), (b) 使用FeBC (a)和FePC (b)降解AO7溶液的颜色变化. (c), (d) FeBC (c)和FePC (d)条带在不同降解时间下AO7溶液的归一化浓度变化<sup>[117]</sup>. (e) A@600薄膜的HRTEM图像, 插图显示了非晶相和晶相的尺寸分布. (f) 588 nm波长附近的归一化吸收强度与处理时间的关系, 插图显示了与商用铁粉的降解行为比较. (g) 染料降解性能比较(不包括Fenton类反应). 不同金属玻璃和晶态零价铁催化剂的降解率与用量比<sup>[118]</sup>

**Figure 7** (Color online) (a), (b) Visible color change of AO7 solution degraded by FeBC (a) and FePC (b) amorphous ribbons. (c), (d) The normalized concentration change of AO7 solutions at different degradation cycles of FeBC (c) and FePC (d) ribbons [117]. (e) HRTEM image of A@600 film, the inset shows the size distribution of the amorphous phase and crystalline phase. (f) Normalized absorption intensities around 588 nm as a function of the treatment time, the inset shows the comparison degradation behavior with commercial Fe powder. (g) Comparison of dye degradation performance (Fenton-like reactions are not included). Degradation rate *versus* dosage ratio for different metallic glasses and crystalline ZVI catalysts [118].

性能和染料降解效率, 是商业铁粉的300倍(图7(e)–(g)). 特别是a/c复合材料无需额外加入H<sub>2</sub>O<sub>2</sub>即可实现出色的催化性能, 这不仅提供了环保的中性催化条件, 还避免了商业污水处理过程中的腐蚀损害.

#### 4 非晶态合金在催化领域面临的问题与展望

催化反应的研究重点是探索高效耐用的催化剂. 虽然大部分研究都集中在晶体材料上, 但非晶态合金

催化剂在降低成本和提高电化学效率方面展现出显著优势. 与晶态催化剂相比, 非晶态合金催化剂具有更多的活性位点, 大量的固有缺陷也有利于提高其催化活性. 这些优点使得非晶态合金在电化学领域具有很强的吸引力. 虽然非晶态合金在催化领域的应用前景广阔, 但相关研究仍处于起步阶段. 可以预见, 随着人们对各种合成方法的掌握, 以及各种高端表征技术的兴起和利用, 非晶态合金催化剂的研究将会取得更多重大进展. 在此, 我们总结了非晶态合金催化剂面临的一些科学问题, 并对未来的研究进行了展望.



(1) 合成方法: 传统的非晶态合金制备方法通常需要高温、高压和复杂的工艺, 这导致了制备过程可控性差和成本较高. 因此, 开发简单、高效且可大规模应用的制备方法是十分重要的. 随着3D打印技术的兴起, 其在材料制备方面具有成本低、精度高和结构可控等优势, 这使得非晶态合金在催化领域的合成技术有望实现突破.

(2) 材料筛选: 目前, 非晶态合金催化剂的研发和设计主要依赖于经验和反复试验. 为了降低成本和缩短实验周期, 机器学习(ML)方法的最新进展已证明其在预测非晶态合金性能方面的有效性和实用性, 特别是在催化剂设计领域. 与第一性原理计算相比, 机器学习方法使物质的采样和分析变得更加广泛和系统. 机器学习是加速催化剂研究的有力工具, 它能够高精度地建立模型, 预测未知催化剂的催化性能, 并揭示催化剂的结构与性能之间的关系. 机器学习模型成功的关键在于使用合适且通用的描述符, 以准确、全面和系统地表示非晶态合金催化剂的结构信息.

(3) 相比于晶态催化剂, 人们对非晶态合金催化剂的认识仍然不够. 虽然大量文献报道了非晶态合金催化剂的催化性能优于同组分的晶态催化剂, 但其确切原因仍然不清楚. 因此, 亟须开发更多先进的表征技术和理论手段, 以探索其结构与催化性能之间的构效关系, 丰富和发展非晶态合金催化剂的物理化学理论.

(4) 原位表征手段: 与晶态催化剂相比, 非晶态合金中缺乏明确的远程有序结构, 这导致催化机理更加复杂. 因此, 需要发展先进的表征技术和理论方法, 以揭示非晶态合金催化剂的催化反应机理. 原位表征技术, 如原位傅里叶变换红外光谱(*in-situ* FTIR)、原位拉曼光谱(*in-situ* Raman)、原位X射线衍射分析(*in-situ*

XRD)、原位透射电子显微镜(*in-situ* TEM)、原位球差校正透射电子显微镜(*in-situ* ACTEM)、原位电子能量损失谱(*in-situ* EELS)、原位X射线光电子能谱(*in-situ* XPS)、原位微分电化学质谱(*in-situ* DEMS)和原位同步辐射(*in-situ* XAS)等, 对于检测催化剂表面关键中间体的吸附和脱附, 以及化学键的形成和断裂至关重要. 这些技术有助于我们更好地了解活性位点的形成和演变, 并在原子尺度上建立精确的结构-性能关系, 解析催化反应的物化机制, 为非晶态合金催化剂的结构优化提供指导.

(5) 定向表面重构: 非晶态物质具有亚稳态结构, 在极端物理或化学条件下易发生表面重构, 转变为晶体结构, 这会影响催化活性和稳定性. 由于非晶态合金在电化学环境中往往会重构生成晶体层, 形成纳米/非晶复合材料, 这极有可能提升电化学性能, 但该过程的不可控性也增加了研究的难度. 因此, 迫切需要从实验结果和理论出发, 发展新的策略, 使非晶态合金催化剂能够定向重构, 从而提升其催化性能和稳定性.

(6) 构筑纳米-非晶异质结: 纳米-非晶异质结催化剂具有独特的结构优势. 非晶结构通常具有更高的表面能和更多的活性位点, 而纳米晶则具有更好的热稳定性和导电性. 通过晶化工程或非晶化工程构筑纳米-非晶异质结构, 或者将非晶态合金与纳米晶材料直接复合以构筑异质结, 结合两者的优点, 可以实现更高效的催化性能.

目前, 对非晶态合金特性的研究大多集中在力学和磁性领域. 近几年的研究表明, 非晶态合金在催化领域表现出优异的性能. 随着非晶态合金在合成、表征和理论计算等方面的快速发展, 预计将在能源储存和转换领域发挥重大作用.

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## Application of amorphous alloys in catalysis

WU Yong & YU Peng\*

*College of Physics and Electronic Engineering, Chongqing Normal University, Chongqing 401331, China*

*\*Corresponding author (email: [pengyu@cqnu.edu.cn](mailto:pengyu@cqnu.edu.cn))*

With economic and population growth, the global demand for energy and the pressure on the environment are rapidly increasing. The over-exploitation and consumption of fossil energy sources have led to a series of problems (such as energy depletion, environmental pollution, and global warming) that seriously endanger the survival and development of humankind. Reducing the utilization of fossil energy sources is the key to achieving carbon neutrality and peak carbon goals. A viable strategy is the development of catalysis, which can produce and store clean, sustainable energy. Different catalytic processes produce sustainable energy sources depending on different reaction mechanisms, but their realization and eventual commercialization rely on the development of high-performance catalysts. Amorphous alloys exhibit a series of excellent mechanical, physical, and chemical properties due to their unique disordered microstructure. Amorphous alloys, as new and efficient catalysts, have a wide range of applications in the field of energy storage and conversion. Compared with crystalline materials, they have the following advantages. (1) Amorphous alloys can adjust their compositional structure within a wide range. (2) Amorphous alloys are isotropic, do not have defects such as grain boundaries and segregation, and have uniform active sites as well as corrosion resistance. (3) Amorphous alloys can be prepared under flexible conditions. (4) Amorphous alloys have a high surface energy as well as a high degree of unsaturated coordination, which enables some chemical reactants and intermediates to be adsorbed on specific sites in an appropriate form. (5) Amorphous alloys have a metastable structure, which is prone to surface reconstruction under extreme physical or chemical conditions, changing from inert species to active-phase species. Amorphous alloys, with their unique structure and performance advantages, make them a catalytic material with great application prospects. This article briefly summarizes the research progress, performance advantages, and application potential of amorphous alloy catalysts. Furthermore, the challenges of amorphous alloy catalysts and their prospects are also summarized.

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