

Condition monitoring and fault diagnosis of industrial robots: A review

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Abstract Health management of industrial robots is paramount for maintaining effective operations, ensuring consistent performance, minimizing downtime, and ultimately enhancing the safety and productivity of robotic systems. Since the invention of industrial robots, significant efforts have been dedicated to their health management. In recent years, thanks to advances in condition monitoring and fault diagnosis technologies of industrial robots, robot health management has shifted from scheduled maintenance to condition-based maintenance. This paper aims to comprehensively review the evolution of condition monitoring and fault diagnosis technologies that are critical for implementing condition-based maintenance of industrial robots. A brief introduction to robotic systems is given first to analyze the robot failure modes and their corresponding root causes. Next, the data acquisition strategies and commonly used sensors of industrial robots are investigated. Further, the development of robot condition monitoring and fault diagnosis technologies are reviewed, with an emphasis on the remarkable achievements and challenges in model-based and data-driven methods. Finally, the paper summarizes the challenges facing this research field and provides potential avenues for future advancements.

Keywords industrial robots, failure modes, data acquisition, condition monitoring, fault diagnosis

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1 Introduction

Over the past few decades, industrial robots (IRs) have made their mark in numerous sectors of modern industry, thanks to their advantages of cost-effectiveness, versatility, and efficiency. Although IRs are more reliable than humans and never get tired or bored with tedious tasks, they do go on strike occasionally due to reliability issues [1]. Scheduled maintenance is a common practice to prevent unexpected shutdowns of IRs. However, the scheduled maintenance of a large stock of IRs always results in resource wastage and even may fail to eradicate potential risks. To overcome the limitations associated with scheduled maintenance, a variety of condition monitoring and fault diagnosis technologies have been developed to realize a paradigm shift toward condition-based maintenance of IRs.

The failure modes of IRs include performance degradation of the overall systems and faults of individual components within the robotic system [2–4]. Therefore, existing studies on the condition monitoring and fault diagnosis of IRs can be categorized into two levels: system level and component level. The former concentrates on the performance evaluation of the entire robotic system, emphasizing positioning accuracy, load capacity, and stability of the overall system of IRs. The latter focuses on the health assessment of components within the robot, highlighting the faults of key components, such as electronic drives, electric motors, speed reducers, and sensors.

In the system-level condition monitoring and fault diagnosis of IRs, model-based methods are widely recognized as the most powerful tools for the detection, isolation, and identification of robot abnormalities, including body collision, driving force losses, and sensing drift [5–8]. Note that the generalized momentum observer-based method, one of

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the typical model-based methods, has been commercialized and integrated into the control systems of numerous IRs for real-time monitoring and diagnosis of robotic systems [9]. In the implementation of model-based methods for condition monitoring and fault diagnosis of IRs, the challenge mainly comes from the unmodelled uncertainties. Indeed, accurate modelling of the nonlinear behaviors of IRs, e.g., deformation, contact, impact, and friction, remains an open problem [10–12].

In the component-level condition monitoring and fault diagnosis of IRs, data-driven methods are becoming increasingly popular with most of them developed in the last five years [13–16]. Key components within IRs, such as speed reducers and electric actuators, are also common in the rotating machinery. Consequently, many studies leveraged the experience gained from fault diagnosis of rotating machinery to develop data-driven fault diagnosis methods for the rotating components in IRs [17–19]. In addition to the problems related to individual components of IRs, there are some robotic-specific challenges in condition monitoring and fault diagnosis of IRs, such as the scarcity of robotic-specific data, dynamic coupling between multiple components, and time-varying configuration of IRs [20–22].

This paper aims to provide a comprehensive overview of the development of condition monitoring and fault diagnosis of IRs and explores future opportunities and challenges in this research area. Compared with the related surveys [3,4,9,13–15,23–25], the primary contributions of this paper are as follows.

(1) This paper systematically investigates the failure modes of IRs, including the faults of robot components and body collision as noted in the existing surveys. Further, the paper discusses the behavior and root causes of the robot failures and summarizes the common faults of robot components in the existing literature.

(2) Data of faulty IRs forms the foundation of the robot health management, yet strategies for data collection are rarely discussed in the existing surveys. This paper highlights the data acquisition of faulty IRs and discusses in detail commonly used data acquisition strategies. Meanwhile, the paper introduces the proprioceptive sensors and investigates the commonly used additional sensors in data acquisition of IRs.

(3) Almost all surveys on model-based condition monitoring and fault diagnosis of IRs are over ten years old. This paper reviews the development of model-based methods in the past 30 years, including the recent advancements made in system modelling, residual generation, and decision-making.

(4) In reviewing the data-driven condition monitoring and fault diagnosis of IRs, this paper distinguishes itself from previous surveys by shifting focus from the types of data-driven methods to an examination of the data sources utilized and the faults addressed by these methods. The literature is

organized into three distinct categories based on the data source: log data, proprioceptive sensor data, and additional sensor data. Such a categorization clarifies the applicability of different data sources for diagnosis of various faults of IRs.

The remainder of this paper is organized as follows. Section 2 illustrates the failure modes of IRs and common faults of robotic components and summarizes the data acquisition strategies of faulty IRs. Section 3 reviews the existing methods for condition monitoring and fault diagnosis of IRs. Further, some practical examples are provided to demonstrate the implementation of model-based and data-driven methods. Section 4 discusses the challenges facing this research field and provides potential avenues for future advancements. Section 5 concludes the paper.

2 Failure modes and data acquisition strategies of industrial robots

The scope of this paper is limited to electrically actuated IRs composed of four subsystems: mechanical system, electrical system, control system, and sensing system. The three concentric rings in Figure 1, from the innermost to the outermost, respectively present the typical mechanical structures, a concise principle of cooperation among subsystems, and some basic components of IRs. Note that the components of IRs are far more diverse than those displayed in Figure 1. The diversity of components and mechanical structures makes IRs adaptable to numerous applications but also poses a great of challenges to the condition monitoring and fault

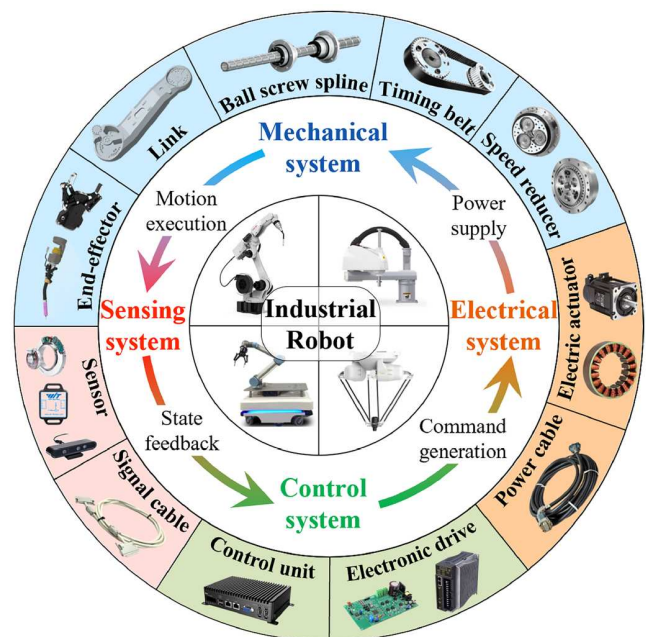


Figure 1 (Color online) System structure and basic components of industrial robots.

diagnosis of IRs. Further, the number of proprioceptive sensors in IRs is far less than the number of components, where most IRs are equipped only with essential sensors for motion control and most components in the mechanical system are sensorless. The above features of IRs make their condition monitoring and fault diagnosis a challenging task. Prior to introducing methods for condition monitoring and fault diagnosis of IRs, this section discusses in detail the failure modes and common faults of IRs, as well as data acquisition of faulty IRs.

2.1 Failure modes and common faults

In the early days of IRs, industrial control devices, such as programmable logic controllers, had just entered the digital age, and the electronic components in controllers were unreliable and subject to frequent failures [26]. At the same time, the primary cause of robot failures was the malfunction of electronic components, leading to the loss of basic functions of IRs. Therefore, the fault diagnosis of electronic components was a major concern in the design of control systems of the old-fashioned IRs [27].

Over the past fifty years, there has been a dramatic transformation in robot hardware and software technologies, significantly improving the reliability of control systems, which now integrate elementary fault diagnosis functions [2,28]. However, manual inspections of IRs are still indispensable to evaluating the health status of sensor-less mechanical systems. Further, it is well-known that the evolution process of faults in mechanical systems is always long-term, and faults in mechanical systems typically result in a degradation of the overall performance of IRs rather than an immediate loss of functions. For example, an unacceptable positioning error of the end-effector caused by faults in the mechanical system is a common failure mode in IRs used for precision machining [29–31]. Thus, failure modes of IRs include not only the loss of basic functions but also the

substandard performance of the overall system.

In addition to the problems from IRs, interferences from the external environment, such as human mistakes, are also major sources of failure of IRs [32–35]. For example, IRs, especially those who frequently interact with the external environment, often fail tasks due to unexpected collisions with their surroundings. In summary, an IR is generally considered a failure if it is unable to complete user-specified tasks. The failure modes of IRs can be broadly categorized into three types: loss of basic functions, substandard performance of the overall system, and external environmental interferences.

All the failure modes of IRs can be isolated to the abnormal behaviors of robot joints and links based on the well-known kinematic and dynamic models of IRs. Further, all the abnormal behaviors of robot joints and links are related to faults or abnormal behaviors of robot components, but relations between them are complex and difficult to model. Therefore, in the existing literature, the abnormal behaviors of robot joints and links are often simulated by modifying the inputs, outputs, or system parameters of IRs. The commonly simulated abnormal behaviors of robot joints and links include free-swinging joints [36], locked joints [37], partial loss of joint driving forces [38], drift in feedback data of joint displacements/speeds [39], and abnormal oscillation of joints and links [40,41].

The complex behaviors of robot joints and links, plus the diversity of robot components and faults, make the fault diagnosis of IRs challenging. Identifying the possible faults of robot components and corresponding abnormal behaviors of the overall system is helpful for the fault diagnosis of IRs, particularly for fault isolation [18–22,42–105]. Table 1 summarizes the common component faults of IRs and corresponding studies that provide experiment results of faulty IRs. Note that, in practice, the component faults of IRs go far beyond those listed in Table 1. Examples include faults of planetary gearboxes used in mobile robots [42], faults of load

Table 1 Common faults of robot components

Components	Faults ^{a)}	References
Servo drive	Inverter fault, capacitor fault, current sensor fault ^{b)}	[50–54]
Permanent magnet synchronous motor	Stator fault, rotor fault, brake fault, bearing fault	[55–66]
Harmonic reducer	Flexible spline fault, circular spline fault, wave generator fault, input shaft fault, manufacturing and assembly error, poor lubricant	[18,22,56,57,63,67–75]
Rotate vector reducer	Sun gear fault, planetary gear fault, crankshaft fault, pin gear fault, cycloidal gear fault, main bearing fault, seal fault, manufacturing and assembly error, poor lubricant	[19,20,70,76–98]
Timing belt	Belt fault, pulley fault	[75,99–101]
Bearing	Fault of support bearings in robot joints	[21,102,103]
Fastener	Bolt loosening of robot joints, bolt loosening of robot base	[104,105]

a) Faults listed in this table can be further subdivided according to their type and degree.

b) Current sensors are typically embedded in servo drives.

balancing mechanisms used in heavy-duty IRs [43], and faults of power cables [44]. Furthermore, there are lots of studies, not explicitly related to robotics, that have investigated the faults of components commonly used in IRs [45–49]. Although most of the fault diagnosis methods developed in these studies are not applicable to IRs, the fruitful experience gained from these studies advances the development of condition monitoring and fault diagnosis of IRs. For example, drawing on the experience gained from fault diagnosis of rotating machinery, many data-driven methods use vibration signals to diagnose the faults of speed reducers and electric actuators in IRs [14].

2.2 Data acquisition

Data acquisition of faulty IRs is both costly and labor-intensive due to the complexity and diversity of robot components. Further, it usually takes years to collect the full lifecycle data of an IR. In the existing studies, the following strategies are commonly used to collect data on faulty IRs: numerical simulation of faulty IRs; manual modification of inputs, outputs, or parameters of actual IRs; replacement of normal (healthy) components of IRs with faulty ones; and accelerated aging tests of IRs or their individual components. Details of these four strategies are given as follows.

(1) Numerical simulation of faulty IRs. The benefits of numerical simulation are economical, efficient, and safe, making it a preferred strategy for the development, debugging, and validation of condition monitoring and fault diagnosis methods for IRs. Since the 1990s, numerical simulation has been accepted by many studies to generate data on faulty IRs [106–109]. Nowadays, a wide range of robot simulation platforms are available, such as Gazebo, Webots, Coppeliassim, Mujoco, Isaac, and Raisim [10]. However, numerical simulation of component faults of IRs remains underdeveloped. For example, the existing studies predominantly employ simple functions such as pulses, steps, and ramps to simulate excitations generated by faulty components of IRs [77,110].

(2) Manual modifications of inputs, outputs, or parameters of actual IRs. Manually modifying robot inputs, outputs, and parameters to simulate faults of actual IRs is cost-effective and easy to implement, since it does not require any hardware modifications. Such a strategy is typically used to simulate anomalies in joint driving forces [36,111–114], anomalies in sensor feedback data [39,115–118], and external disturbances [119–123]. For example, the free-swinging actuation failure can be simulated by setting the reference torque to zero and the drift in sensor data can be simulated by introducing an additive signal to the measured data. However, it is impossible by far to simulate all component faults of IRs without hardware modifications. For example, modifications of robot inputs, outputs, and para-

meters are unable to simulate the stochastic excitations introduced by faults of speed reducers, which involve complex behaviors that are not yet understood thoroughly [124–126]. Further, modifications of robot inputs, outputs, and parameters could make IRs unstable and even pose risks to operators, especially in human-robot interaction scenarios [122].

(3) Replacement of normal components of IRs with faulty ones. In robotic factories, there are many substandard components of IRs retired from actual industrial lines. It is therefore cost-effective to obtain faulty IRs by replacing the components of normal IRs with substandard ones. For example, many studies employed faulty speed reducers and motors obtained from actual industrial lines to collect data on faulty IRs [20,64,65,67–69]. Fault injection is another way to obtain faulty components of IRs. The existing studies focused on fault injection of rotating machinery of IRs, including rotate vector (RV) reducers [19,79–83], harmonic reducers [70,75], and timing belts [75,99–101]. Most existing studies chose to inject faults into the rotating machinery of IRs for two main reasons: frequent impact and contact in rotating machinery make it susceptible to wear and tear, and IRs are able to work with faulty mechanical components.

(4) Accelerated aging tests of IRs or their individual components. It is time-consuming and costly to collect full lifecycle data of IRs. For example, Vallachira et al. [127] spent over four years collecting full lifecycle data of 26 IRs worked in actual industrial lines, where 13 IRs were reported with gearbox failures and the rest were normal. Accelerated aging tests are therefore usually employed to expedite the acquisition of full lifecycle data of IRs and their components. Indeed, accelerated aging tests of IRs are also time-consuming, typically taking at least three months [87,88,94,128]. In addition to accelerated aging tests of IRs, a few studies have conducted accelerated aging tests of individual components of IRs, where the test duration is significantly reduced by increasing the load of components. For example, as reported in refs. [53,129–131], accelerated aging tests of harmonic reducers and electronic drives were generally completed within a few days.

Among the above four strategies, the numerical simulation strategy is the most flexible, allowing to read any data available in the simulation model of IRs. In the remaining three strategies, the type of data that can be obtained depends on the sensors that the robot is equipped with. In most IRs, states of electric actuators obtained by proprioceptive sensors can be read through the control system. Further, additional sensors are usually employed to assist the proprioceptive sensors in acquiring data from actual IRs. One of the key issues in using additional sensors is sensor selection, where the following factors need to be considered: (i) costs of adding sensors, (ii) faults needed to be diagnosed, (iii) reliabilities of additional sensors, and (iv) operating

conditions of additional sensors [87,132]. The application of additional sensors in condition monitoring and fault diagnosis of IRs is discussed in detail in subsections 3.2.3 and 3.3.2.

3 Condition monitoring and fault diagnosis technologies

The existing methods for condition monitoring and fault diagnosis of IRs can be broadly categorized into three types: knowledge-based methods, model-based methods, and data-driven methods. Expert knowledge permeates the entire lifecycle of IRs, from design and manufacturing to service and maintenance. During the design phase, a systematic analysis of failure modes and effects offers essential insights for condition monitoring and fault diagnosis of IRs [133]. The knowledge accumulated from condition monitoring and fault diagnosis is then fed back into the design and manufacturing processes to eliminate potential flaws. Expert knowledge of condition monitoring and fault diagnosis forms knowledge-based methods. Further, the development of both model-based and data-driven methods leverages a rich pool of expert knowledge, effectively integrating most knowledge-based approaches. This section therefore incorporates knowledge-based methods into the review of model-based and data-driven methods.

3.1 Model-based methods

Model-based methods use analytical redundancy to replace hardware redundancy to address condition monitoring and fault diagnosis issues of practical systems [134,135]. Main tasks of model-based condition monitoring and fault diagnosis include system modelling, residual generation, and decision making.

3.1.1 System modelling

The aim of system modelling is to find a mapping between the inputs and outputs of actual systems. Typically, IRs are equipped with rotary encoders and current sensors to measure angular displacements and driving torques of electric motors, respectively. Dynamic models of IRs, that are able to characterize the relationship between angular displacements and driving torques of electric motors, are therefore common in condition monitoring and fault diagnosis of IRs. In some specific scenarios, dynamic models are not the only option for condition monitoring and fault diagnosis of IRs where the robot or its surrounding environment is equipped with additional sensors. For example, in visual servoing applications, IRs are typically equipped with vision sensors. In such cases, it is able to assess the health status of IRs using the robot kinematic models that characterize the relationship

between the measurements of proprioceptive and additional sensors [136–138]. This paper focuses on the dynamic modelling of IRs, and readers interested in other models are referred to ref. [2].

The well-known rigid-body dynamic is widely used to characterize the dynamic behavior of IRs with high stiffness [139,140]. However, rigid-body dynamics often fail to characterize the dynamic behaviors of IRs with elastic joints or long arm spans, such as collaborative robots. Various rigid-flexible coupling models were introduced in existing studies to address the flexibilities of IRs [9,141,142]. The trade-off between computational efficiency and numerical accuracy is a big issue in the existing studies of flexible body modelling, where most rigid-flexible coupling models are too complicated to be both computationally efficient [143]. Further, there are many unresolved issues in the parameter identification of flexible body models [144]. Besides flexibility in IRs, modelling and parameter identification of nonlinear characteristics introduced by contact, collision, friction, and clearance between multiple components are also challenging [77,145].

Around 1990, neural networks were introduced into the dynamic modelling of robots to learn nonlinear behaviors [146]. Nevertheless, the learning abilities of early neural networks are not powerful enough to achieve the performance of traditional physical models in many scenarios. After more than twenty years of revolution, the advent of deep learning brought rapid progress to neural networks. For example, the popular physics-inspired neural networks of recent years have made significant breakthroughs in robot dynamics learning and interpretability [147–150]. However, the practical implementation of physics-informed neural networks still faces many limitations, such as their performance being highly dependent on the chosen application object, as well as the quality and quantity of training data [143]. Readers are recommended to refer to refs. [148,151] for the details of recent advances in learning-based modelling methods for robot dynamics. Furthermore, a systematic review of learning-based methods applied to the modelling and identification of general dynamic systems can be found in ref. [152].

3.1.2 Residual generation

In model-based condition monitoring and fault diagnosis, residual generation is a process of using the known nominal models to find a residual that contains information of faults on actual systems [6]. Studies on model-based condition monitoring and fault diagnosis of IRs can be classified into three categories based on their residual generation approaches: parameter identification methods, parity space methods, and state estimation methods.

(1) Parameter identification methods

Parameter identification-based residual generation meth-

ods make use of the fact that faults of actual systems often lead to changes in the values of model parameters [106,153]. The primary tasks of parameter identification-based residual generation methods include model selection and parameter identification. A necessary condition for model selection is that at least one of the identifiable parameters reflects the fault of actual systems. In practice, model selection depends on the expert knowledge of actual systems and it is usually not easy to find a model with identifiable parameters that are both sensitive to faults and robust to disturbances. One of the challenges in model selection is that most model parameters are coupled with each other and cannot be identified individually. For example, most parameters of dynamic models of IRs are not individually identifiable due to the complex robot structure and scarcity of proprioceptive sensors [154]. Further, model parameters that carry information on robot faults are typically time-varying and depend on the operating conditions of the robot. For example, the stiffness and friction coefficients of robot joints that are able to reflect faults of speed reducers are influenced by various factors, such as the spatial configuration and trajectory of the robot, and environmental conditions [77].

Parameter identification of robot models is also challenging due to unmodelled dynamics and measurement uncertainties. Common methods to cope with unmodelled dynamics and measurement uncertainties in parameter identification include extended Kalman filter [155,156], maximum likelihood estimation [157,158], set membership estimation [159,160], instrumental variable method [161,162], and semi-definite programming method with physically feasible constraints [163–166]. Among the above methods, adding reasonable constraints based on the expert knowledge of the actual robot is the only way to obtain physically feasible estimates of all model parameters [167]. However, obtaining accurate estimates of all model parameters remains by far a challenging task due to the inherent nonlinear dynamics of IRs. For example, Bittencourt et al. [94,128] used friction models to estimate the wear of robot joints, where the displacement, speed, load, and temperature of robot joints, as well as the temperature of the lubricant, have to be simultaneously recorded to determine the parameters of friction models.

In practice, parameter identification methods are more commonly used in residual generation in combination with other model-based methods than in isolation. For example, many studies employed parameter identification and state estimation methods to design adaptive observer for residual generation [110,168–171]. Indeed, since some parameters of robot models are time-varying, parameter identification methods are essential for almost all the model-based residual generation methods.

(2) Parity space methods

Parity space-based residual generation methods take ad-

vantage of the parity relations of inputs and outputs of the actual systems. Around 1980, the parity space-based residual generation methods were first introduced to linear systems in two forms: direct redundancy and temporal redundancy [172]. The direct redundancy depends on the parity relations among instantaneous inputs and outputs and the temporal redundancy depends on the parity relations among historical inputs and outputs. Based on the linear forms of parity space methods, Leuschen et al. [173,174] developed a nonlinear analytic redundancy method for the residual generation of a planar robot, where the robot model is assumed to be consistent with the actual robot. Further, Halder and Sarkar [117,175] proposed a robust nonlinear analytic redundancy method to minimize the effects of model-plant-mismatch on the generated residuals by solving a nonlinear optimization problem. Their method was verified by experiments on a PUMA 560 robot, where faults were simulated by manually modifying actuator inputs and sensor outputs. Another way to improve the robustness of the generated residuals is to increase the order of parity relations [176,177]. However, the order of parity relations is also limited by some practical issues, such as noise amplification and huge computation burden [113]. It is therefore of primary interest to generate a residual with the lowest possible order of parity relations that is able to detect faults.

Since parity space methods excel at redundancy analysis of sensor outputs, they are usually used to aid other model-based methods for designing residuals. For example, Frank et al. [107,123] employed parity space methods to design state observers for residual generation and applied the generated residual to detect the collision of robots.

(3) State estimation methods

State estimation methods are the most popular residual generation methods in condition monitoring and fault diagnosis of IRs [8,9]. The key idea of state estimation methods is to design observers or filters that reconfigure the inputs and outputs of IRs to generate residuals. Depending on the model used, state estimation methods can be classified into three categories: physical model-based methods, neural network-based methods, and hybrid model-based methods.

Physical model-based state estimation methods commonly used in the residual generation of IRs include direct estimation [178–180], time-delay estimation [8,181], recursive estimation [8,39,182–184], adaptive estimation [110,120,168,169,185–191], Kalman filter [192–194], Luenberger observer [107,195–203], high-gain observer [204], sliding mode observer [115,116,205–218], unknown input observer [115,205,206,218–220], disturbance observer [217], H-infinity based observer [221–223], energy-based observer [9,224], velocity observer [9,225–231], and momentum observer [9,141,170,197,211,223,232–236]. Among the above methods, the momentum observer method has been commercially applied to many collaborative IRs. A

detailed comparison of the state estimation methods can be found in refs. [9,237,238]. Due to the difficulty in accurately modelling the inherent nonlinear characteristics of IRs, model-plant-mismatch remains one of the unsolved challenges of physical model-based state estimation methods.

Around 2000, neural networks were introduced into robot modelling, which led to the development of neural network-based state estimation methods. Since then, numerous studies used state estimation methods based on shallow neural networks, such as Hopfield network, radial basis function network, and multi-layer perceptron with one hidden layer, for residual generation of IRs [239–251]. Given the limited capability of shallow networks in learning robot dynamics, many studies developed hybrid model-based state estimation methods for the residual generation of IRs by combining neural networks with physical models [112,252–259]. In recent years, deep learning has revolutionized robotics. Deep neural networks provide better approximations of the nonlinear dynamics of IRs compared to shallow neural networks [148]. Alongside deep learning, reinforcement learning is also gaining momentum in the field of robotics. However, the application of deep learning and reinforcement learning for state estimation-based residual generation of IRs is still in its early stages with only a few relevant studies [14,15]. For example, Sacchi et al. [206] used a state estimation method based on deep reinforcement learning to design residuals for a robot with sensor faults.

3.1.3 Decision making

The process of determining the health status of IRs through residual evaluation is known as decision-making, which involves fault detection, fault isolation, and fault identification. The decision-making methods in condition monitoring and fault diagnosis of IRs can be broadly categorized as threshold-based and learning-based methods.

(1) Threshold-based methods

The basic idea of threshold-based methods is to compare the raw or post-processed residuals with specified thresholds to detect faults of IRs. In general, multiple residuals and associated thresholds are required to achieve fault isolation of IRs [153]. For example, many studies combined multiple residual generators to develop a general diagnostic framework capable of addressing multiple faults of IRs simultaneously [194,197,209,218,221,222,260]. Further, the residuals are affected by model and measurement uncertainties that vary with the operating conditions of IRs. It is therefore a challenging task to determine thresholds for numerous residuals of IRs. To address the above issues, the existing studies on residual evaluation of IRs have tried numerous methods to determine thresholds, including expert knowledge-based methods, statistics-based methods, and fuzzy logic-based methods.

Expert knowledge-based methods are typically used to

determine thresholds for the IRs whose dynamics are well-understood. For example, the residual thresholds can be determined using interval estimation methods when the bounds of the model and measurement uncertainties of the robot are known [108,114,191,261]. For the IRs with unknown models and measurement uncertainties, statistics-based methods are commonly used to determine the residual thresholds. In such cases, extensive experiments on the IRs are required to figure out the statistical properties of residuals since model and measurement uncertainties vary with the operating conditions of IRs [8,39,112,171,182]. Among statistics-based methods for determining thresholds of IRs, a commonly used method is to set the threshold as the maximum of the corresponding residual. However, fixed thresholds are too conservative to detect incipient faults. Therefore, many studies introduced fuzzy logic-based methods to adaptively update the threshold according to the operating conditions of IRs [123,231,241,242]. Additionally, proper post-processing of residuals also helps avoid conservative thresholds. For example, in collision detection of IRs, high-pass filtering of residuals is able to weaken the influence of model uncertainties [9,262].

(2) Learning-based methods

Learning-based methods address decision-making as a classification problem. They are capable of learning the features of different faults from the raw residuals of IRs, avoiding the difficulties associated with the post-processing of residuals and determination of numerous thresholds. However, machine learning-based methods also have limitations, such as they typically require a comprehensive fault dataset for training the classifier.

Numerous studies have shown that the traditional learning-based method, such as learning methods based on radial basis function networks, multilayer perceptron, support vector machines and k -nearest neighbours, achieve high accuracy in residual classification of IRs [207,239,240,246,247,249–251,254,263,264]. The primary reason for this success is that the residual generation incorporates extensive expert knowledge of the robot faults, along with preliminary treatment of the model and measurement uncertainties of the robot. This makes the generated residuals sensitive to faults, enabling learning-based methods to effectively extract features of faults from the raw residuals.

Terra and Tinós [246] compared a learning method based on radial basis function networks and a threshold-based method for the actuator fault diagnosis of a robot. Their experimental results demonstrated that the learning method based on radial basis function networks is more robust to perturbations than the threshold-based method. Park et al. [265] used a learning method based on support vector machines and convolutional neural networks to classify momentum residuals of a robot to detect collisions. The results showed that the learning method based on convolutional

neural networks outperformed the learning method based on support vector machines when the number of training samples was sufficient. Considering the high cost of collecting robot fault data, Park et al. [266] introduced unsupervised learning for residual classification to reduce the dependence on large amounts of labelled fault data. Additionally, Kim et al. [267] employed a transfer learning method for residual classification to facilitate the sharing of fault data and knowledge across multiple robots.

3.2 Data-driven methods

The data obtained from proprioceptive sensors, event logs from the control system and maintenance logs are typically available for condition monitoring and fault diagnosis of IRs. However, log data and proprioceptive sensor data are obviously insufficient for the condition monitoring and fault diagnosis of all components of IRs. Adding sensors to IRs is therefore a common practice to enhance data acquisition of their components, particularly for the sensorless components. Based on the available data for IRs, three categories of data-driven condition monitoring and fault diagnosis methods have been developed: methods based on log data, methods based on proprioceptive sensor data, and methods based on additional sensor data.

3.2.1 Methods based on log data

Robot log data mainly includes event information such as warnings and alarms from controllers and electronic drives. In practice, robot maintenance experts often begin their troubleshooting with the above log data, leveraging expert knowledge to investigate the causes of faults. They further enrich their expert knowledge based on collected historical log data and maintenance records. Manually refining expert knowledge is time-consuming and labour-intensive, prompting many studies to use techniques like natural language processing to refine knowledge from log data and maintenance records. Knowledge graphs, known for their powerful information organization and association abilities, are particularly favoured for the refinement and management of fault diagnosis knowledge of IRs [268]. For example, Wang et al. [269–271] utilized deep learning methods to extract semantic entities and relationships from log data, maintenance records, and repair manuals of IRs. They constructed a fault diagnosis knowledge graph for the robot fault isolation and maintenance decision-making. Due to the difficulty of fault isolation caused by the rich semantic relations in the knowledge graph, Li et al. [272,273] integrated methods like fuzzy decision-making into the fault diagnosis knowledge graph to analyze the root causes of faults of IRs.

Given the lower sampling frequency of log data compared to proprioceptive sensor data, log data is generally used for fault isolation and cause analysis in fault diagnosis, while

proprioceptive sensor data is mainly used for online fault detection. For example, the predictive maintenance system for welding robots developed by Wang et al. [60] first extracts fault characteristics from proprioceptive sensor data to identify the robot's health status. When a fault is detected, the log data is recorded and input into the fault diagnosis knowledge graph for fault isolation, cause analysis, and maintenance decision-making.

3.2.2 Methods based on proprioceptive sensor data

The proprioceptive sensor data can be accessed through the control system of IRs at sampling frequencies ranging from 1 Hz to 7000 Hz [274]. The proprioceptive sensor data of IRs typically includes angular displacements, angular speeds, currents, and torques of electric motors. In recent years, numerous data-driven methods based on proprioceptive sensor data have been developed for condition monitoring and fault diagnosis of IRs.

One of the most intuitive data-driven methods is to directly compare proprioceptive sensor data from normal and faulty IRs. Such methods are generally applicable to IRs that perform repetitive tasks [275]. For example, Izagirre et al. [55] achieved the fault diagnosis of a robot by comparing joint torques under identical motion trajectories. They validated their method on a heavy-duty IR that unexpectedly shut down on a production line. Upon disassembly, it was discovered that the shutdown was due to a significant increase in joint torques caused by a fault in the motor brake. Xiao et al. [276,277] detected the abnormal vibrations or noise of different robot joints by comparing the proprioceptive sensor data from normal and faulty IRs under the same motion trajectory. They also investigated the effect of data sampling frequency on fault detection. Their experiment results show that the classification accuracy of faults in the robot joints remains high even at a sampling frequency of 0.1 Hz. Chen et al. [56,57,63,64,278] collected proprioceptive sensor data from IRs with single and compound faults by replacing faulty motors and speed reducers with normal ones. They demonstrated that faults in electric motors and speed reducers of IRs can be diagnosed using data-driven methods based on deep learning and the proprioceptive sensor data with a sampling frequency of 1 Hz. Yang et al. [72] utilized proprioceptive sensor data from an IR under a single-joint reciprocating motion to identify abnormal vibrations induced by the harmonic reducer in the robot joint. Similarly, Hsu et al. [100] employed proprioceptive sensor data from an IR under a single-joint reciprocating motion to detect the timing belt looseness in the robot joint.

Considering the difference between online operating trajectories and offline test trajectories, Oh et al. [20] implemented fault diagnosis of IRs using transfer learning and proprioceptive sensor data under multiple trajectories for both reciprocating motions of a single-joint and those of

multiple joints. Heo et al. [279] used deep learning and proprioceptive sensor data to detect the collision of a robot that executes randomly generated motion trajectories, where the robot is required to repeatedly follow these trajectories. In summary, existing data-driven condition monitoring and fault diagnosis methods necessitate robots repeatedly executing specific motion trajectories. When it comes to a new trajectory, most data-driven algorithms require fine-tuning or even retraining based on the proprioceptive sensor data of the new trajectory.

3.2.3 Methods based on additional sensor data

One of the advantages of data-driven methods based on additional sensor data is that sensors can be customized to the specific faults of IRs. Due to the diversities of faults of IRs, a variety of sensors have potential applications in condition monitoring and fault diagnosis of IRs. Table 2 summarizes the additional sensors that are commonly used in the existing studies of IRs, with most of the references published within the last five years [18,19,21,22,34,44,61,62,65–70,73–76,78–92,95,97–99,102–105,118,185,205,262,280–305]. As shown in Table 2, accelerometers are the most frequently used additional sensors in data acquisition of IRs, followed by current sensors and inertial measurement units (IMUs). The popularity of accelerometers is due to two main reasons: mechanical systems of IRs have many rotating components and accelerometers are widely accepted for condition monitoring and fault diagnosis of rotating machinery [17]. Current sensors are also popular for condition monitoring and fault diagnosis of rotating machinery driven by electric motors [274]. Although the proprioceptive sensors of IRs include current sensors, the stator currents obtained by them are generally not publicly accessible. Therefore, many studies added current sensors to IRs to collect stator currents of electric motors. In the following sections, all current sensors

refer to additional current sensors unless otherwise specified. IMUs added to IRs are usually used to estimate motion states of links, such as spatial poses, speeds, and accelerations [2]. With the motion states of links, it is thereby able to evaluate the overall performance of entire systems of IRs, as well as to estimate the motion states of robot joints by solving inverse kinematics problems [136]. In addition to accelerometers, current sensors and IMUs, some studies have employed other sensors, such as cameras, acoustic emission (AE) sensors, microphones, and laser trackers, to estimate the states of IRs. A detailed discussion of applications of the additional sensors in condition monitoring and fault diagnosis of IRs is given in the sequel.

(1) Accelerometers

As shown in Table 2, accelerometers are the most used additional sensors in condition monitoring and fault diagnosis of IRs. They are typically mounted on the robot joints and links to acquire vibration data of the rotating components at sampling frequencies greater than 1 kHz.

Numerous studies have employed the vibration data obtained by accelerometers to diagnose faults in mechanical power transmission components of IRs. For example, Nentwich et al. [88,281,283] mounted accelerometers on IRs to collect the full life cycle data under accelerated wear. They analyzed the effects of temperature and mounting position on the vibration data obtained by accelerometers and verified the feasibility of using vibration data to diagnose faults of gearboxes in the robot joints. He et al. [18,67–69] fixed an accelerometer on each link of a 6-degrees-of-freedom (DOF) IR to collect vibration data and used deep learning methods to diagnose artificial faults of harmonic reducers at different operating speeds of the robot joints. Yang et al. [22,73,74,282] orthogonally mounted three unidirectional accelerometers at the end-effector of a 6-DOF IR and achieved abnormal vibration detection of harmonic reducers

Table 2 Additional sensors commonly used in IRs

Sensors	Advantages	Disadvantages	References
Accelerometer	• Sensitive to faults of rotary machine • Low cost • Easy to install	• Trajectory dependent • Placement dependent	[18,19,21,22,61,67–69,73–76,78,81–83,85–88,91,98,99,102–104,262,280–290]
Current sensor	• Sensitive to faults of electric motors, electronic drives, proprioceptive current sensors, and power cables	• Trajectory dependent • Friction dependent	[44,62,65,70,78,87,99,102,105,291–293]
IMU	• Sensitive to faults of rotary machine • Able to track the pose of IRs	• Calibration required for pose tracking • Prone to drift	[79,80,84,89,90,92,95,185,294,295]
Camera	• Images are intuitive and interpretable	• Light dependent • Calibration required for pose tracking • High cost	[34,66,118,205,296–301]
AE sensor	• Sensitive to incipient faults of machinery	• Placement dependent • Extremely high sampling frequency	[97,102,302,303]
Microphone	• Large measurement range	• Sensitive to noise • Trajectory dependent	[19,304]
Laser tracker	• High-accuracy pose measurement of IRs	• Extremely high cost • Stringent measurement conditions required	[305]

in three joints close to the end-effector. Pu et al. [76,81,85,86] mounted an accelerometer on a link of a 6-DOF IR and used deep learning methods to detect artificial faults of an RV reducer connected to the link. Note that although the above studies using accelerometers for fault diagnosis of IRs achieve high accuracy close to 100%, most of them require the robot to follow specific motion trajectories [20].

Considering the effect of time-varying operating conditions on the vibration response of IRs, Kim et al. [98] used the joint velocities obtained by proprioceptive sensors to split the vibration data obtained by accelerometers. Further, they analyzed the spectral characteristics of the vibration data under the uniform motion of the robot joint to diagnose the faults of the RV reducer. Qiao et al. [78] combined accelerometers and current sensors to synchronously collect vibrations and stator currents in a robot joint. They achieved fault diagnosis of RV reducers at time-varying speeds and loads using nonlinear response spectrum analysis of current and vibration data. In addition to fault diagnosis of speed reducers, vibration signals from accelerometers had also been applied to fault diagnosis of electric motors [61], timing belts [75], and bolts [104,284], as well as collision detection of links [262,285].

(2) Current sensors

The primary advantage of adding current sensors to IRs is the ease of installation. Most Hall current sensors allow the power cable of the robot to pass through for measuring the stator currents of electric motors. This enables the use of current data obtained by current sensors to diagnose faults of power cables [44]. The stator currents measured through the power cable serve as both the output of the electronic drive and the input to the electric motor, making them useful for diagnosing faults of electronic drives [54,306,307] and electric motors [62,291]. Furthermore, additional current sensors provide hardware redundancy with the proprioceptive current sensors within the electronic drive and can be used for fault diagnosis of sensors. In fact, faults of proprioceptive current sensors can also be identified by current signature analysis even without hardware redundancy since the three-phase stator windings of an electric motor are typically symmetrical [306,307].

Due to the compact structure of IRs, the torsional characteristics of the speed reducers also affect the dynamic response of the electric motors. Consequently, the stator current data of the motor are often used to diagnose faults of speed reducers in the robot joints [293]. For example, Liu et al. [77] developed a dynamic model of IRs to analyze the effects of faults and nonlinear behaviors of RV reducers on motor performance. They further demonstrated the feasibility of using motor currents or torques for long-term health monitoring of RV reducers in robot joints. Additionally, many data-driven methods have employed motor currents obtained by additional current sensors to diagnose faults of

harmonic reducers and RV reducers [70]. Since motor current reflects the health state of speed reducers primarily through torsional characteristics, this method is insensitive to partial faults of speed reducers and susceptible to frictional perturbations. Therefore, some studies have proposed fault diagnosis methods that integrate multiple sources of data, such as current, vibration, and acoustic emission, to identify the health status of speed reducers in robot joints [78,102]. In fact, in a robot joint, the dynamic response of the motor is affected by many factors other than faults of speed reducers, such as loose bolts and lubricant leakage. For example, Xu et al. [105] verified the feasibility of using motor currents obtained by additional current sensors to identify bolt loosening of a robot joint.

(3) IMUs

In condition monitoring and fault diagnosis of IRs, IMUs that consist of accelerometers, gyroscopes, and magnetometers are generally fixed to the robot links to acquire their linear acceleration, angular velocity, and orientation at a sampling frequency of less than 1 kHz [308]. Given that the robot links are driven by robot joints, the fault diagnosis of components in robot joints can be performed using the motion data of links. For example, many studies mounted IMUs on the robot links to collect their motion data and utilized the link motion data to diagnose faults of the RV reducer connected to the link [79,80,84,89,90,92]. These studies employed deep learning methods to extract fault features of RV reducers from the link motion data where the robot is required to follow specific motion trajectories.

In addition to fault diagnosis of components, IMUs are also common in collision detection and system performance evaluation of IRs. For example, Birjandi et al. [294] mounted an IMU at the end-effector of a 6-DOF robot and performed collision detection of links by fusing data obtained from the IMU and proprioceptive sensors. In their work, the precise calibration of the position of the IMU relative to the robot link is required to accurately estimate the collision force. Similarly, the calibration of IMUs is also crucial for estimating the end-effector positioning errors of IRs [295,309,310].

(4) Cameras

Cameras are common in visual-servoing applications and environmental monitoring of IRs. There are two configurations of IRs and cameras, namely the eye-in-hand configuration and the eye-to-hand configuration [2]. The camera-based condition monitoring and fault diagnosis of IRs usually performed in the eye-to-hand configuration where cameras are fixed in the robot workspace to capture the image of IRs and their surroundings. For example, Peng and Chen [298] utilized images captured by cameras fixed in the workspace of IRs to estimate their actual positions and compare the actual positions with the desired/commended ones to detect malfunctions of the robot. At the same time,

the images captured by cameras can also be used to detect anomalies of other objects in the robot workspace [296,311]. In addition to 2D images, depth cameras, such as structured light cameras, are able to produce depth data that can be used to estimate distance between two entities in 3D space. Typical applications of depth cameras in condition monitoring and fault diagnosis of IRs include collision detection [312], positioning error evaluation [118,297,299–301], and fault diagnosis of actuators and sensors [205]. Note that the calibration of cameras is required for almost all applications, especially for the positioning error evaluation of high-accuracy IRs.

(5) AE sensors

Thanks to the ability to detect transient elastic stress waves generated by the deformation of materials, AE sensors are more sensitive to incipient faults of machinery compared to accelerometers, current sensors, IMUs, and cameras [49]. In the condition monitoring and fault diagnosis of IRs, AE sensors are typically used to detect faults of bearings and speed reducers [97,102,302,303]. The frequency of acoustic emissions produced by speed reducers in IRs can reach hundreds of kilohertz, necessitating a high sample frequency for AE sensors and resulting in a significant computational burden for signal processing.

(6) Microphones

In the manual maintenance of IRs, experienced engineers identify the health status of speed reducers by listening to the sounds they make during operation. Inspired by this practice, some studies used microphones to collect sounds produced by IRs for condition monitoring and fault diagnosis. For example, Qiao et al. [19] used a microphone and an accelerometer to diagnose the faults of an RV reducer in single joint robot, where the microphone was fixed near the RV reducer and the accelerometer was fixed on the RV reducer. They discovered that combining sound and vibration data for fault diagnosis of RV reducers yields better results than using either data source alone. Yun et al. [304] attached microphones to the links of a six-DOF IR to identify abnormal noises caused by overloading. In their experiment setup, the microphones were securely fixed to the link surfaces to minimize external sound interference. Similar to accelerometers, the condition monitoring and fault diagnosis of IRs using microphones generally require the robot to respectively execute specific trajectories.

(7) Other sensors

In addition to the six commonly used sensors mentioned above, other types of sensors such as temperature sensors and voltage sensors have also been used in condition monitoring and fault diagnosis of IRs. For example, Sabry et al. [313] added voltage and current sensors to a robot's electronic drive to monitor power consumption, which in turn was used to diagnose the actuator and sensor faults of the robot. Temperature sensors were usually used to help

monitor the wear of speed reducers of IRs [94,128].

Although there are abundant sensors available for condition monitoring and fault diagnosis of IRs, sensors capable of accurately measuring the pose of the robot end-effector online are scarce. The commonly used sensors for the pose measurement of IRs include laser trackers, draw-line encoders, IMUs, and cameras. While laser trackers and draw-line encoders offer high-accuracy pose measurement, their stringent measurement conditions and high costs make them impractical for online pose measurement of most IRs in real-production lines [314]. IMUs and cameras are not as accurate as laser trackers and draw-line encoders for position measurement, but they are cost-effective. Applications of IMUs and cameras in online pose measurement of IRs are also challenging due to their inherent drawbacks, such as drift of IMUs, and the light-dependency of cameras.

3.3 Practical examples

This subsection presents some practical examples to briefly demonstrate the implementation of model-based and data-driven methods for condition monitoring and fault diagnosis of IRs. In the demonstration of the model-based methods, the dynamic model of IRs is first introduced followed by the implementation of parameter identification methods, parity space methods, and state estimation methods. The demonstration of data-driven methods is organized into two parts: (1) data acquisition and (2) data analysis.

3.3.1 Model-based methods

In general, the dynamic models of a n -degrees-of-freedom robot can be written as a set of second-order differential equations of the form [274]:

$$\mathbf{M}(\mathbf{q}, \mathbf{p})\ddot{\mathbf{q}} + \mathbf{C}(\mathbf{q}, \dot{\mathbf{q}}, \mathbf{p})\dot{\mathbf{q}} + \mathbf{g}(\mathbf{q}, \mathbf{p}) + \mathbf{f}(\mathbf{q}, \dot{\mathbf{q}}, \mathbf{p}) = \boldsymbol{\tau}, \quad (1)$$

where $\mathbf{q}, \dot{\mathbf{q}}, \ddot{\mathbf{q}} \in \mathbb{R}^n$ are generalized position, velocity, and acceleration vectors, respectively. $\mathbf{p}$ is a vector of model parameters that collects geometric parameters, inertial parameters, friction parameters, and so on. $\boldsymbol{\tau} \in \mathbb{R}^n$ is a vector of applied forces. $\mathbf{M}(\mathbf{q}, \mathbf{p}) \in \mathbb{R}^{n \times n}$ is a symmetric and positive-defined matrix of inertia terms. $\mathbf{C}(\mathbf{q}, \dot{\mathbf{q}}, \mathbf{p})\dot{\mathbf{q}}$ is a vector of the Coriolis and centrifugal force terms with $\mathbf{C} \in \mathbb{R}^{n \times n}$ and $\dot{\mathbf{M}} = \mathbf{C} + \mathbf{C}^T$. $\mathbf{g}(\mathbf{q}, \mathbf{p}) \in \mathbb{R}^n$ is a vector of gravitational terms. $\mathbf{f}(\mathbf{q}, \dot{\mathbf{q}}, \mathbf{p}) \in \mathbb{R}^n$ is a vector of force terms that account for any other forces acting on the system other than those in $\boldsymbol{\tau}$ (e.g., friction forces, disturbances generated by speed reducers and electric actuators). It is well-known that $\mathbf{f}(\mathbf{q}, \dot{\mathbf{q}}, \mathbf{p})$ is typically challenging to model accurately. Therefore, implementing model-based methods requires extensive attention to address the modelling errors associated with $\mathbf{f}(\mathbf{q}, \dot{\mathbf{q}}, \mathbf{p})$.

In most IRs, $\mathbf{q}$ and $\boldsymbol{\tau}$ are measurable. $\dot{\mathbf{q}}$ and $\ddot{\mathbf{q}}$ can be obtained by numerically differentiating the measured $\mathbf{q}$ once

and twice. Note that special attentions are always required to address the noise in $\ddot{\mathbf{q}}$ and τ .

(1) Parameter identification methods

Combining the robot dynamic equations of K samples yields a set of nonlinear equations of $\mathbf{p}$. The estimates of model parameters are then obtained by solving the nonlinear equations of $\mathbf{p}$. Such a process is known as the parameter identification. Define a simple residual based on parameter identification as

$$\mathbf{r}_{PI} = |\hat{\mathbf{p}} - \mathbf{p}_0|, \quad (2)$$

where $\mathbf{p}_0$ and $\hat{\mathbf{p}}$ are the nominal values and current estimates of model parameters, respectively.

In the fault-free case, $\mathbf{r}_{PI}$ is expected to be zero. However, the unmodelled dynamics and measurement uncertainties of real IRs always make $\mathbf{r}_{PI}$ greater than zero. Therefore, in fault detection of IRs, a lot of experiments are required to determine robust thresholds for each term in $\mathbf{r}_{PI}$. Further, the fault isolation and fault identification of IRs are also possible by examining each term in $\mathbf{r}_{PI}$. A detailed illustration of parameter identification-based fault diagnosis methods can be found in ref. [106] and a review of parameter identification methods can be found in ref. [167].

(2) Parity space methods

Parity space methods rely on past measurement and input data from the actual system, making them primarily applicable to discrete-time dynamic systems. Additionally, determining the parity vector in these methods requires the state space equations of the actual system. Define the state variables of the robot as

$$\mathbf{x} = \begin{bmatrix} \mathbf{q} \\ \dot{\mathbf{q}} \end{bmatrix}. \quad (3)$$

The state space equations of the dynamic model of a n -degrees-of-freedom robot are given by

$$\dot{\mathbf{x}} = \mathbf{A}_c \mathbf{x} + \mathbf{B}_c \tau + \mathbf{h}_c + \eta_c \quad (4)$$

with

$$\mathbf{A}_c = \begin{bmatrix} 0_{n \times n} & 1_{n \times n} \\ 0_{n \times n} & 0_{n \times n} \end{bmatrix}, \mathbf{B}_c = \begin{bmatrix} 0_{n \times n} \\ \mathbf{M}^{-1}(\mathbf{x}, \hat{\mathbf{p}}) \end{bmatrix},$$

$$\mathbf{h}_c = \begin{bmatrix} 0_{n \times n} \\ \mathbf{M}(\mathbf{x}, \hat{\mathbf{p}})^{-1} \mathbf{N}(\mathbf{x}, \hat{\mathbf{p}}) \end{bmatrix}, \mathbf{N}(\mathbf{x}, \hat{\mathbf{p}}) = \mathbf{C}(\mathbf{x}, \hat{\mathbf{p}}) \dot{\mathbf{q}} + \mathbf{g}(\mathbf{x}, \hat{\mathbf{p}}) + \mathbf{f}(\mathbf{x}, \hat{\mathbf{p}}).$$

In eq. (4), $\eta_c \in \mathbb{R}^{2n}$ denotes the modelling uncertainties. According to the first order forward Euler's method, the discrete-time form of eq. (4) with a fixed time step T can be written as

$$\mathbf{x}(k+1) = \mathbf{A} \mathbf{x}(k) + \mathbf{B}(k) \tau(k) + \mathbf{h}(k) + \eta(k) \quad (5)$$

with

$$\mathbf{A} = \begin{bmatrix} 1_{n \times n} & T 1_{n \times n} \\ 0_{n \times n} & 1_{n \times n} \end{bmatrix}, \mathbf{B}(k) = \begin{bmatrix} 0_{n \times n} \\ T \mathbf{M}^{-1}(\mathbf{x}(k), \hat{\mathbf{p}}) \end{bmatrix},$$

$$\mathbf{h}(k) = \begin{bmatrix} 0_{n \times n} \\ T \mathbf{M}^{-1}(\mathbf{x}(k), \hat{\mathbf{p}}) \mathbf{N}(\mathbf{x}(k), \hat{\mathbf{p}}) \end{bmatrix}, \eta(k) = T \eta_c(k) + \rho(k),$$

where $\rho(k)$ represents the discretization errors due to the truncation of the series.

Introducing the actuator faults and sensor faults into the robot dynamics yields

$$\begin{aligned} \mathbf{x}(k+1) = & \mathbf{A} \mathbf{x}(k) + \mathbf{B}(k) (\tau(k) + \mathbf{f}_a(k)) \\ & + \mathbf{h}(k) + \eta(k) + \mathbf{f}_s(k), \end{aligned} \quad (6)$$

where $\mathbf{x}(k)$ and $\tau(k)$ are the actual values of $\mathbf{x}(k)$ and $\tau(k)$ of faulty robots, respectively. $\mathbf{f}_a(k) \in \mathbb{R}^{2n}$ and $\mathbf{f}_s(k) \in \mathbb{R}^{2n}$ are vectors account for the effects of actuator faults and sensor faults on the robot dynamics.

Combining eq. (6) of K samples yields

$$\bar{\mathbf{x}}_K = \mathbf{A}_K \bar{\mathbf{x}}(1) + \mathbf{B}_K (\bar{\tau}_K + \mathbf{f}_{a,K}) + \mathbf{C}_K (\bar{\mathbf{h}}_K + \bar{\eta}_K + \mathbf{f}_{s,K}) \quad (7)$$

with

$$\bar{\mathbf{x}}_K = \begin{bmatrix} \bar{\mathbf{x}}(2) \\ \bar{\mathbf{x}}(3) \\ \vdots \\ \bar{\mathbf{x}}(K) \end{bmatrix}, \bar{\tau}_K = \begin{bmatrix} \tau(1) \\ \tau(2) \\ \vdots \\ \tau(K-1) \end{bmatrix},$$

$$\mathbf{f}_{a,K} = \begin{bmatrix} \mathbf{f}_a(1) \\ \mathbf{f}_a(2) \\ \vdots \\ \mathbf{f}_a(K-1) \end{bmatrix}, \mathbf{h}_K = \begin{bmatrix} \mathbf{h}(1) \\ \mathbf{h}(2) \\ \vdots \\ \mathbf{h}(K-1) \end{bmatrix},$$

$$\mathbf{f}_{s,K} = \begin{bmatrix} \mathbf{f}_s(1) \\ \mathbf{f}_s(2) \\ \vdots \\ \mathbf{f}_s(K-1) \end{bmatrix}, \bar{\eta} = \begin{bmatrix} \eta(1) \\ \eta(2) \\ \vdots \\ \eta(K-1) \end{bmatrix},$$

$$\mathbf{A}_K = \begin{bmatrix} \mathbf{A} \\ \mathbf{A}^2 \\ \vdots \\ \mathbf{A}^{K-1} \end{bmatrix}, \mathbf{C}_K = \begin{bmatrix} 1_{2n \times n} & 0_{2n \times n} & \cdots & 0_{2n \times n} \\ \mathbf{A} & 1_{2n \times n} & \cdots & 0_{2n \times n} \\ \vdots & \vdots & \ddots & \vdots \\ \mathbf{A}^{K-2} & \mathbf{A}^{K-3} & \cdots & 1_{2n \times n} \end{bmatrix},$$

$$\mathbf{B}_K = \begin{bmatrix} \mathbf{B}(1) & 0_{2n \times n} & \cdots & 0_{2n \times n} \\ \mathbf{A} \mathbf{B}(1) & \mathbf{B}(2) & \cdots & 0_{2n \times n} \\ \vdots & \vdots & \ddots & \vdots \\ \mathbf{A}^{K-2} \mathbf{B}(1) & \mathbf{A}^{K-3} \mathbf{B}(2) & \cdots & \mathbf{B}(K-1) \end{bmatrix}.$$

Define the residual as

$$\begin{aligned} \mathbf{r}_{PS} = & \mathbf{V} (\bar{\mathbf{x}}_K - \mathbf{A}_K \bar{\mathbf{x}}(1) - \mathbf{B}_K \bar{\tau}_K - \mathbf{C}_K \bar{\mathbf{h}}_K) \\ = & \mathbf{V} (\mathbf{B}_K \mathbf{f}_{a,K} + \mathbf{C}_K \bar{\eta}_K + \mathbf{C}_K \mathbf{f}_{s,K}) \end{aligned} \quad (8)$$

with

$$\mathbf{r}_{PS} = \begin{bmatrix} r_{PS,1} \\ r_{PS,2} \\ \vdots \\ r_{PS,s} \end{bmatrix}, \mathbf{V} = \begin{bmatrix} \mathbf{v}_1^T \\ \mathbf{v}_2^T \\ \vdots \\ \mathbf{v}_s^T \end{bmatrix},$$

where $\mathbf{v}_i \in \mathbb{R}^{2n(K-1)}$ ($i = 1, 2, \dots, s$) is known as the parity vector.

In the actuator fault diagnosis, $\mathbf{v}_i$ is expected to satisfy

$$\mathbf{v}_i \mathbf{B}_K \neq 0, \mathbf{v}_i \mathbf{C}_K = 0. \quad (9)$$

In practice, it is impossible to find $\mathbf{v}_i$ that always satisfies eq. (9). The above desired property can be weakened to the following statement: finding a set of vector $\mathbf{v}_i$, such that $\|\mathbf{v}_i \mathbf{B}_K\|$ is far more than $\|\mathbf{v}_i \mathbf{C}_K\|$. Such a statement means that the residual is much more sensitive to actuator faults than to modelling errors and sensor faults.

In the sensor fault diagnosis, $\mathbf{v}_i$ is expected to satisfy

$$\mathbf{v}_i \mathbf{B}_K = 0, \mathbf{v}_i \mathbf{C}_K \neq 0, \mathbf{v}_i \mathbf{C}_K \boldsymbol{\eta}_K = 0. \quad (10)$$

Similarly, the above desired property can also be weakened to the following statement: finding a set of vector $\mathbf{v}_i$, such that $\|\mathbf{v}_i \mathbf{C}_K\|$ is far more than $\|\mathbf{v}_i \mathbf{B}_K\|$ and $\|\mathbf{v}_i \mathbf{C}_K \boldsymbol{\eta}_K\|$. Readers who are interested in the implementation of other forms of parity space methods are suggested to refer to refs. [117,315].

(3) State estimation methods

The design of state observers is key to the implementation of state estimation-based fault diagnosis methods. According to ref. [8], the general structure of state observer for the robot dynamics given in eq. (6) can be written as

$$\begin{aligned} \hat{\mathbf{x}}(k+1) &= \mathbf{A}\hat{\mathbf{x}}(k) + \mathbf{B}(k)\hat{\boldsymbol{\tau}}(k) + \mathbf{h}(k) \\ &\quad + \hat{\boldsymbol{\eta}}(k) + \mathbf{K}_0 \mathbf{e}(k) \end{aligned} \quad (11)$$

with

$$\mathbf{e}(k) = \mathbf{x}(k) - \hat{\mathbf{x}}(k), \mathbf{K}_0 = \begin{bmatrix} \mathbf{K}_1 & T\mathbf{1}_{n \times n} \\ 0_{n \times n} & \mathbf{K}_2 \end{bmatrix},$$

where $\mathbf{K}_1 \in \mathbb{R}^{n \times n}$ and $\mathbf{K}_2 \in \mathbb{R}^{n \times n}$ are positive definite diagonal matrices and are also called the gain matrices.

In eq. (11), $\hat{\mathbf{x}}(k)$ is the estimate of state variable $\mathbf{x}(k)$ and $\hat{\boldsymbol{\eta}}(k)$ is the estimate of modelling error $\boldsymbol{\eta}(k)$. The recursive equations for $\mathbf{e}(k)$ is given by

$$\begin{aligned} \mathbf{e}(k+1) &= \mathbf{x}(k+1) - \hat{\mathbf{x}}(k+1) \\ &= \mathbf{F}_0 \mathbf{e}(k) + \hat{\boldsymbol{\eta}}(k) + \mathbf{B}(k)\mathbf{f}_a(k) + \mathbf{f}_s(k), \end{aligned} \quad (12)$$

where $\hat{\boldsymbol{\eta}}(k) = \boldsymbol{\eta}(k) - \hat{\boldsymbol{\eta}}(k)$ and $\mathbf{F}_0 = \mathbf{A} - \mathbf{K}_0$.

Define a residual as

$$\begin{aligned} r_{\text{SO}}(k+1) &= \mathbf{e}(k+1) - \mathbf{F}_0 \mathbf{e}(k) \\ &= \hat{\boldsymbol{\eta}}(k) + \mathbf{B}(k)\mathbf{f}_a(k) + \mathbf{f}_s(k). \end{aligned} \quad (13)$$

It is clear that $r_{\text{SO}}(k+1)$ is affected by the estimation error of the modelling error $\boldsymbol{\eta}(k)$. The typical estimation methods for $\boldsymbol{\eta}(k)$ can be found in refs. [8,238]. Note that regardless of how $\boldsymbol{\eta}(k)$ is estimated, only fault detection can be achieved using $r_{\text{SO}}(k+1)$. A further process of $r_{\text{SO}}(k+1)$ is required to achieve fault isolation and fault identification. Such a limitation can be addressed by combining the state estimation

methods and parity space methods, e.g., using the parity space methods to design a transformation matrix for $r_{\text{SO}}(k+1)$. Furthermore, the state observer given in eq. (11) has an inherent limitation: the requirement to calculate the inverse of the inertia matrix $\mathbf{M}(\mathbf{q}, \hat{\mathbf{p}})$. Such a limitation was addressed by Luca and Mattone [234], where they proposed the well-known momentum observer based on the property of robot dynamics $\dot{\mathbf{M}}(\mathbf{q}, \mathbf{p}) = \mathbf{C}(\mathbf{q}, \dot{\mathbf{q}}, \mathbf{p}) + \mathbf{C}^T(\mathbf{q}, \dot{\mathbf{q}}, \mathbf{p})$. Readers are recommended to refer to refs. [9,313] for the details of the implementation of momentum observer and other observers in fault diagnosis of IRs.

In practice, the combination of the above three categories of model-based methods is common in the condition monitoring and fault diagnosis of IRs. The advantages of combining parameter identification methods, parity space methods, and state estimation methods are as follows. (i) Model parameters can be continuously updated using parameter identification methods to account for the time-varying terms in robot dynamics, in particular the force term $\mathbf{f}(\mathbf{q}, \dot{\mathbf{q}}, \mathbf{p})$ in eq. (1); (ii) Parity space methods can be employed to design the state observer-based residuals that are sensitive to faults and robust to disturbances; (iii) Residual generation can be performed online using state estimation methods to ensure a numerically stable and efficient computation.

3.3.2 Data-driven methods

(1) Data acquisition

In this subsection, a six-degrees-of-freedom serial robot is taken as an example to demonstrate the acquisition of log data, proprioceptive sensor data, and additional sensor data. The experiment setup of the robot is presented in Figure 2. All joints of the robot are driven by electric motors equipped with two types of proprioceptive sensors: the high-resolution encoders and the phase current sensors. The proprioceptive encoders and proprioceptive current sensors are used to measure the positions and stator currents of electric motors, respectively. All the proprioceptive sensor data is fed back to the robot control unit to enable close-loop control of electric motors. Meanwhile, the log data is also recorded in the robot control unit. Note that the maximum sample frequency of proprioceptive sensor data is 1000 Hz and the log data is event-triggered data.

In addition to the proprioceptive sensor, two types of additional sensors, accelerometers and current sensors, are added to the robot. As shown in Figure 2, accelerometers are fixed on the robot links to collect vibration data. The additional current sensors are employed to measure the stator currents of electric motors with the power cable of the robot passing through the current sensors. Further, a multi-source data acquisition device is required to collect the additional sensor data at adjustable sample frequencies. The determination of sample frequency of additional sensor data depends

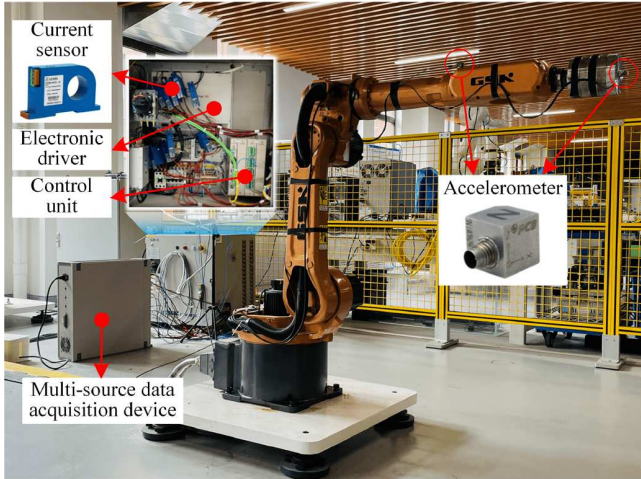


Figure 2 (Color online) Experimental setup of a six-degrees-of-freedom robot for data acquisition.

on many practical requirements, where the following factors need to be carefully considered: (i) fault excitation bandwidth; (ii) sensor bandwidth; (iii) computation and storage requirements; and (iv) associated costs.

In addition to the sensor selection, the choice of exciting trajectories is also a key issue in the data acquisition of IRs. Different from the traditional rotating machinery, the choice of exciting trajectories of IRs must account for numerous physical constraints, such as the position limits of robot joints. As depicted in Figure 3, these physical constraints necessitate frequent acceleration and deceleration of the robot joints during operation, resulting in significant variations in the joint positions, velocities, and torques. Further, the robot configuration, i.e., the poses of robot joints and links, also varies with the motion of the robot. Note that the time-varying configuration of robots not only has great influences on the joint torques but also alters the pose of additional sensors fixed on the robot links. All the above characteristics of IRs pose a great of challenges to data acquisition and analysis. Consequently, the existing studies on condition monitoring and fault diagnosis of IRs often require IRs to follow specific motion trajectories.

(2) Data analysis

The data analysis of IRs typically involves three main procedures: (i) data pre-processing; (ii) feature extraction; and (iii) fault diagnosis. The key issues in the implantation of these procedures are discussed as follows.

The synchronization of multi-source data, including proprioceptive sensor data, log data, and additional sensor data, is of paramount importance in the data pre-processing of IRs. As displayed in Figure 2, the additional sensor data is collected by a multi-source data acquisition device, while the proprioceptive sensor data and log data are collected by the robot control unit. The synchronization between the robot control unit and the multi-source data acquisition device is

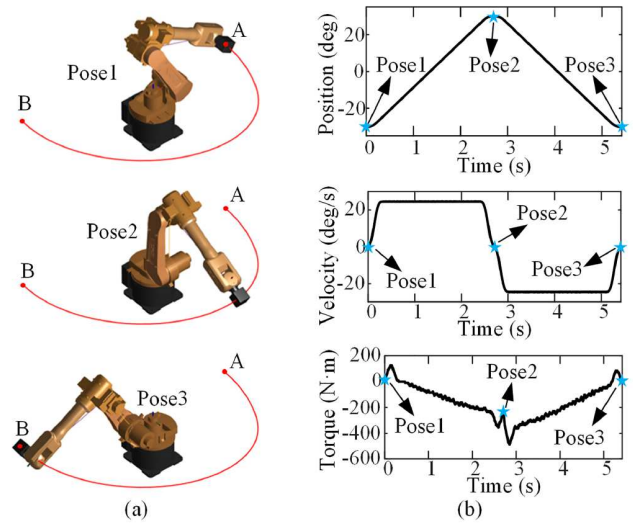


Figure 3 (Color online) Exciting trajectory of a six-degrees-of-freedom robot. (a) The robot end moves back and forth between point A and point B; (b) the output positions, velocities, and torques of joint 2.

therefore required to allow the data acquisition of proprioceptive and additional sensors to begin at the same time. In practice, the robot control unit can be programmed to send a digital trigger signal to the multi-source data acquisition device when data collection begins and stops. Further, parts of the multi-source data can also be synchronized through data analysis [316].

The main challenge in feature extraction of robot data comes from the time-varying operation conditions of IRs. One approach to address this challenge is to extract the stationary data when the robot joint velocity is constant. Once stationary data is obtained, typical signal processing techniques can be employed to extract features in the time domain, frequency domain, and time-frequency domain [17]. Another common approach is using neural networks to extract features from data of IRs with time-varying operation conditions. Note that the features extracted by neural networks lack clear physical interpretation and are usually not generalized across different trajectories of IRs [20]. In other words, when the robot executes a new trajectory, the neural network used for feature extraction needs to be retrained with data from the new trajectory.

The fault diagnosis of IRs consists of three key tasks: fault detection, fault isolation, and fault identification. Generally, fault detection is easy to be achieved through data analysis when the robot follows a specific trajectory. For example, it is able to detect the faults of components in the robot joint by comparing the proprioceptive sensor data obtained from the normal and faulty robots. An example is depicted in Figure 4, where the robot follows the exciting trajectory displayed in Figure 3(a). It is obvious that the joint torques of normal and faulty robots are quite different, where notable periodic fluctuations can be found in the joint torque of the faulty

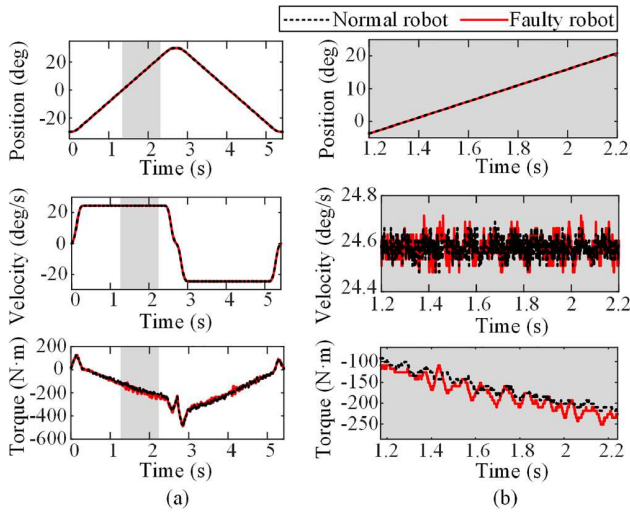


Figure 4 (Color online) Comparison of proprioceptive sensor data obtained from the normal and faulty robots. (a) The output positions, velocities, and torques of joint 2; (b) local view of the output positions, velocities, and torques of joint 2.

robot. The periodic fluctuations are generated by the faults of the RV reducer in joint 2. Therefore, the faults of the RV reducer in joint 2 can be detected by comparing the joint torques of normal and faulty robots.

In the implementation of fault isolation, fusion of multi-source data is generally essential since there are numerous exciting sources in IRs. The fusion approaches of multi-source data can be broadly classified into the following categories: (i) data-level fusion; (ii) feature-level fusion; and (iii) decision-level fusion. The data-level fusion approaches require synchronization and alignment of data streams and are often applied to the sensors that measure the same or complementary phenomena. For example, the fusion of vibration data obtained by multiple accelerometers fixed on the robot links. The feature-level fusion approaches reduce the dimensionality of multi-source data, focusing on key information. For example, the fusion of frequency-domain features of data measured by multiple accelerometers and current sensors. The decision-level fusion approaches allow for the integration of different types of sensors that are not be compatible at the data- and feature-level. In the decision-level fusion strategy, each sensor provides a separate decision or classification. In such cases, all the sensors, including proprioceptive sensors and additional sensors, can be integrated together to achieve THE isolation of multiple faults of IRs.

The fault identification of IRs using data-driven methods remains an open challenge. To address this issue, it is essential to collect extensive sensor data from a wide range of IRs with various levels of faults. Additionally, a comprehensive understanding of the dynamic behaviors of both normal and faulty IRs is also crucial to identifying the re-

lationships between sensor data and specific faults.

4 Challenges and prospects

4.1 Challenges

Based on the survey of existing methods and practical examples presented in the last section, this section examines the challenges related to condition monitoring and fault diagnosis of IRs from five key aspects: complex structures and numerous components, complex dynamics, complex operating conditions, various failure modes, and weak sensing ability.

(1) Complex structures and numerous components

Various types of IRs have emerged in the industry to adapt to different task requirements. Depending on the kinematic structure, IRs can be classified into serial, parallel, and hybrid types. The condition monitoring and fault diagnosis methods of IRs generally need to be customized to the robot structure. For example, the system performance evaluation and fault isolation methods need to be tailored to the robot structure since the source of positioning errors of a robot is related to the robot structure.

Further, even IRs with the same structure can have different components due to differences in workspace and load capacity. For example, light-weight IRs typically use harmonic reducers, while heavy-load IRs mostly use RV reducers. Different components typically have unique dynamic characteristics, requiring individualized condition monitoring and fault diagnosis methods. The diversity in structures and components makes the data acquisition, system modeling, and customization of condition monitoring and fault diagnosis methods costly and labour-intensive. This is evidenced by the scarcity of experimental data on faults of serial IRs, despite the fact that serial IRs have been a primary focus of robot condition monitoring and fault diagnosis for the past 30 years.

(2) Complex dynamics

Speed reducers provide IRs with powerful load capacity and reliable positioning accuracy but also introduce nonlinear characteristics to the robot system, such as contact, collision, flexibility, backlash, and friction. The time-varying excitation caused by the inherent nonlinearity of speed reducers is often coupled with fault excitation, posing significant challenges to the condition monitoring and fault diagnosis of speed reducers. Additionally, the joint structure of IRs is typically compact. Such compact structure makes the nonlinear behaviors of speed reducers affect not only the performance of electric motors but also the system performance of IRs. Since the nonlinear behaviors of speed reducers and the flexibility of robot links are difficult to model accurately, the system performance evaluation of IRs in real-time is therefore challenging. Consequently, a precise pose

measurement sensor is essential for accurately estimating the positioning errors of IRs.

(3) Complex operating conditions

The complexity of operating conditions of IRs is mainly reflected in two aspects: the time-varying motion states and complex surroundings. The motion process of IRs involves continuous changes in the spatial configuration of the overall system. Correspondingly, motion states such as joint angular displacement, speed, acceleration, and torque are constantly changing. The time-varying characteristics of these motion states make the robot's dynamic responses complex, presenting obstacles to the extraction of fault features.

Further, the condition monitoring and fault diagnosis of IRs are also affected by their complex surroundings. For example, time-varying temperature and humidity of the environment affect the lubricant properties of speed reducers, electromagnetic radiation affects the performance of electronic components, etc. For IRs that interact with the external environment, they have to comply with the motion constraints and loads imposed by the environment. For example, in robotic grinding applications, motion constraints of the robot end-effector change with the surface morphology of the workpiece, and the reaction force from the workpiece can cause abnormal behaviors of the robot, such as the oscillation of robot links. The variety of internal and external time-varying excitations mentioned above poses significant challenges to the condition monitoring and fault diagnosis of IRs, particularly fault isolation and identification.

(4) Various failure modes

The complexity of failure modes in IRs is mainly influenced by two factors: the compact structure and the diversity of components. Clearly, the more components, the more failure modes of IRs. Table 1 lists about thirty common component faults of IRs documented in existing studies, each of them can be further subdivided into various specific fault types. For example, the sun gear fault of RV reducers includes tooth cracking, tooth pitting, tooth spalling, tooth wear, tooth chipping, tooth profile error, misalignment, etc. [317].

The compact structure of IRs means that each component affects the others during operation. For example, wear and tear of speed reducers due to poor lubrication tend to increase the friction forces and temperature of speed reducers, which subsequently elevates the current and temperature of electric motors. This, in turn, causes the current of electronic drives to rise, ultimately leading to the degradation of multiple components within the robot system. These characteristics of IRs—compact structure and numerous components—result in complex failure modes, making the identification of the root cause of failures and the degradation patterns of the entire system a challenging task.

(5) Weak sensing ability

The cost of IRs is a critical factor in determining the fea-

sibility of implementing robotic automation in manufacturing processes. To maintain cost-effectiveness, IRs often have limited proprioceptive sensors and relatively low data sampling frequencies. This setup results in weak sensing abilities of IRs, leading to the following issues for condition monitoring and fault diagnosis: (i) The number of sensors is much fewer than the components of the robot, making fault localization and quantitative fault evaluation difficult; (ii) Proprioceptive sensors are typically located at the motor end, which means they may not effectively detect faults in other components of the robot; (iii) Data collected at low frequencies may miss high-frequency information crucial for diagnosing certain types of faults; (iv) Performance evaluation of the overall system of IRs, such as the positioning accuracy of the robot end-effector, necessitates an accurate robot model.

Additional sensors can be integrated into IRs to improve their sensing ability, but this introduces further considerations: (i) Careful cost-benefit analyses of adding sensors to IRs for condition monitoring and fault diagnosis are required to justify the potential benefits against added expense; (ii) More sensors make the robot system more complex, where additional sensors introduce additional faults to the entire system; (iii) Using additional sensors to collect intensive data of numerous faults of IRs is essential to understand the intrinsic relationship between faults of IRs and responses of additional sensors; (iv) The scarcity of cost-effective pose measurement sensors that is able to simultaneously offer large measurement ranges, high accuracy, and real-time tracking capability without altering operating conditions of IRs.

4.2 Prospects

Addressing the reliability issues of IRs necessitates advancements across multiple facets of robotics: modelling, sensing, planning, control, prognostics, and health management. This section explores the potential avenues to deal with the current challenges from five aspects: sensing ability, robotic-specific dataset, fault mechanism, multimodal model, and digital twin.

(1) Sensing ability

Enhancing the sensing ability of IRs is an intuitive way to address the challenges related to condition monitoring and fault diagnosis. For existing IRs, adding sensors is the primary approach to improve their sensing ability. The optimal selection of additional sensors is crucial to find a low-cost and reliable solution. Meanwhile, it is important to develop pose measurement sensors with a large measuring range, high accuracy, and high reliability to enable real-time measurement of the pose of IRs. For future IRs, it would be interesting to develop robot components with self-sensing abilities. Such self-sensing components not only simplify the

health monitoring of themselves but also facilitate the performance evaluation of the overall system.

(2) Robotic-specific dataset

Data scarcity is a significant challenge in the condition monitoring and fault diagnosis of IRs, highlighting the need to establish robotic-specific datasets of normal and faulty IRs. Clearly, data collection of real-world IRs that encompass various structures, faults, and operating conditions is a reliable way to establish robotics datasets. Meanwhile, simulations of normal and faulty IRs are also worth investigating to efficiently expand the quantity of robotics datasets, with careful attention to narrow the gap between simulation and reality. Further, a thorough investigation into data cleaning and data labelling is also essential to ensure the quality of the robotics datasets.

(3) Fault mechanism

Fault mechanism analysis of IRs, which aims to explain the causes and manifestation of faults, is essential for addressing issues related to fault diagnosis, fault simulation, and optimal selection of sensors. There is no doubt that extensive experimental data on IRs and their components are required to understand the nonlinear behaviors of IRs. Combining models based on physical laws, statistics, and neural networks remains by far an effective approach to understanding and learning the nonlinear behaviors of IRs, with particular attention to the complex behaviors involving contacts and friction.

(4) Multimodal model

Multimodal models are increasingly popular for processing data from multiple sources. They have the potential to provide a comprehensive understanding of the health status of IRs by integrating diverse types of data, including data from various proprioceptive and additional sensors, as well as logs and manual maintenance records. Further, the development of large multimodal models is particularly promising for diagnosing numerous faults simultaneously in IRs, especially when multiple faults emerge concurrently.

(5) Digital twin

The digital twin of IRs, functioning as a virtual representation of the physical robotic systems, facilitates real-time monitoring and predictive maintenance. Given the diverse degradation patterns and health assessment criteria of IRs across various applications, the development of task-specific digital twin systems shows great potential. By tailoring the digital twin systems to specific tasks, they can deliver reliable and computationally efficient health management services for IRs in actual industry.

5 Concluding remarks

This paper presents a comprehensive review of condition monitoring and fault diagnosis of IRs, highlighting both

challenges and achievements in model-based and data-driven methods. Through examination of the existing literature, the paper analyses various failure modes of IRs and the root causes of robot failures. Meanwhile, the data accessible to IRs and the commonly used additional sensors have been explored, with accelerometers being the most popular, followed by current sensors and IMUs. Based on the knowledge of faults of IRs and available data, the paper delves into the current state of model-based and data-driven methods for condition monitoring and fault diagnosis. Further, some open issues are outlined, such as model uncertainties, data scarcity, and dependence on operating conditions. Finally, the paper summarizes the challenges in addressing these open issues and discusses promising pathways for future progress. We hope these insights will inspire readers who are interested in this research field to develop new targeted solutions.

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