

温度对成品油管道顺序输送过程的影响研究进展

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摘要 温度梯度是传热传质过程的动力来源之一, 顺序输送本质上是传热与流动、传质的耦合过程. 当前, 对混油拖尾现象、与热力耦合的调度方法、管内三维传热传质模拟、考虑油品质量潜力的批次跟踪的相关研究中大多未考虑温度的影响也未阐明温度的作用机制. 本文总结了未充分考虑温度影响的管输油品相关研究(混油、调度、热油管道、批次跟踪)的现状和局限性. 评述了考虑温度对混油机理影响、温度对管输过程流动传热传质影响的国内外研究成果, 并梳理了相关的实验研究. 最后指出了水热力耦合的调度、考虑温度影响的反常扩散、可压缩多相紊流的三维数值模拟、复杂管道中的批次跟踪是该领域今后研究的关键问题和发展方向.

关键词 顺序输送, 温度, 批次跟踪, 混油, 传热传质耦合

管道运输已经成为国际成品油运输的发展趋势, 管道运输具有运输量大、占地少、密闭安全、受气候及外界影响小、环境污染小、易于管理和运输成本低等优点^[1]. 中国成品油管道在近十余年间发展迅速. 中国石油天然气集团公司(中石油)的管道公司、西北管道分公司和西南管道分公司拥有兰成渝、兰郑长、北疆、乌兰和港枣等成品油管道逾7000 km. 中国石油化工集团公司(中石化)拥有华北、华中、华东和华南四大成品油管网, 运营里程近8000 km. 中国海洋石油总公司(中海油)、中国中化集团公司(中化集团)也在规划建设成品油管道, 到“十二五”末, 中国成品油管道里程将突破30000 km^[2]. 成品油管道正向网络化发展, 华南已经初步形成枝状、环状、甚至网状的复合型成品油管网, 具有多点进出、多油品和多复杂分支的特点. 但用管道输送成品油的油品种类还相对较少, 输油管网自动化控制、调度系统及混油控制技术还有待发展^[3]. 批次计划自动制定、顺序输送的

运行模拟及批次界面跟踪技术也有待提高. 模拟成品油管道顺序输送时的批次运移过程对于编制最佳调度计划、跟踪混油界面运动、优化运行及确保安全十分重要. 在顺序输送过程中, 随着各批次油品在管内的运行, 各批次的纯油体积、批次间的混油长度及混油浓度均发生变化. 但目前管道沿线的各批次油品的准确位置、纯油段与混油段的长度体积、油品的混合情况等信息无法快速准确获取, 与之相关的各批次油品的质量指标参数亦无法及时获取, 只能通过相关理论计算得到预测值, 这很大程度上影响了成品油管道的数字化、自动化和智能化运行. 管道运行过程中的状态参数、运行参数、技术指标和质量指标等的预测值往往与实际值相差较大, 且为了安全起见预测值常偏于保守. 原因在于目前在做长输成品油管道的水力计算、批次计划、调度计划、混油体积和泄漏检测等时, 认为管道内油品处于平均温度状态, 将整条管道或分段当作等温管道处理. 在计算

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和检测顺序输送产生的混油时也不考虑温度的影响,只在检测混油界面的仪器或设备内设置温度补偿功能^[4-6]。但实际管道运行时,油品在管内流动时的温度一直处于不断变化中。这种温度变化既与管外的温度场有关,也与管内的流动特性有关,还与输送油品的管道以及油品本身的物理特性及初始状态等有关。在站内时这种温度变化还与泵的压缩、泵内摩擦、阀门节流等有关。油品的温度会受到长输过程中所有与之接触的设备、操作以及环境的影响,同时还与其他状态参数耦合在一起。温度既影响前期计划制定、水力计算,中期的分输、注入、输量调节等运行方案操作,也影响后续的油品交割和可能存在的意外事故的处理。因此在跟踪顺序输送油品的界面位置时、接收油的过程中、以及判断是否存在油品泄漏时,均需要正确检测油品温度,以确定油品物性的变化过程,从而计算分析相关的流动参数、状态参数、技术和质量指标值^[7],进而采取相应措施以减小误差或损失^[1,8-10]。

理论研究及数值模拟研究温度对长距离管输流体的影响主要集中在原油管道、液化天然气管道、超临界CO₂管道,温度对管网的影响则集中于供热管道,对针对成品油管道顺序输送管道的研究较少。原因在于温度的影响于前四者是决定性因素,而对于成品油管道温度是重要影响因素。在现在建设数字化和智能化管道运行平台的趋势下,考虑温度对成品油顺序输送的影响也变为必须解决的问题。以往学者于成品油顺序输送的相关研究主要集中在编制批次调度计划、批次位置跟踪模拟、开泵方案优化、混油形成规律和泄漏检测等方面,均没有严格考虑温度的影响。实验研究也集中于流态、油品种类和管道参数对混油量的影响,尚未考虑温度在其中的作用和影响机制。

1 顺序输送成品油制定调度计划时不考虑温度的影响

现有研究在做成品油管道的调度计划时认为管道处于常温运行,不考虑周围环境变化、管道换热情况、摩擦生热等对管道沿线温度的影响。对纯油段和混油段的体积与位置的模拟跟踪预测误差一般在40~60 min^[2],若发生输油计划临时变更、现场执行误差或意外停输等事件,由于没有快速的界面跟踪校

对调整措施,界面跟踪误差会进一步放大甚至达2 h^[1,2]。目前,国内外学者均是以油品库存量、库存成本、泵站运行费用或输送成本总和最小为目标函数,考虑油品供给及需求约束、油品排序限制、质量平衡、管道与站场的注入与分输需求、管道输送能力以及库存约束等条件,建立一种基于已知条件和参数的管道调度启发式模型,制定出一段时间内的输送计划。Shah^[11]研究了原油港口至炼厂原油管道的调度问题,Sasikumar等人^[12]研究了连接炼厂至油库的单一管道系统,Rejowski和Pinto^[13-15]研究了将炼厂的油品在指定时间内运移至多个油库的管道运输问题,Cafaro等人^[16]研究了单注入点、多个分输点的成品油管道系统,Abriza等人^[17]在Pinto所建模型基础上研究了连接油田、炼厂及分输点的管网系统内油品的运输问题,Hane^[18]和Jittamai^[19]分别研究了多种油品顺序输送的时间窗分配问题。梁静华等人^[20]对成品油管道顺序输送时制定调度计划做了基础研究,梁永图等人^[21-23]建立了带有油品分输需求时间窗的成品油管道调度优化问题的整数线性规划模型,宋飞等人^[24]研发了兰成渝管道调度计划编制软件,张强等人^[25]结合主时步法与变时步法改进了调度计划的算法,范华平^[26]建立了自动编制成品油管道分输计划的数学模型。可以看出,无论是对象(管道或管网),还是模式(单源单汇、单源多汇、多源单汇或多源多汇),抑或功能(编制调度计划或优化调度计划),他们的模型和算法中均未考虑温度的影响,只将混油段当作指定长度(批次界面进出站前后各两小时内流过的油品),或用经验公式简单计算后当作无法下载的新增批次,未对温度引起批次界面跟踪的误差进行研究,因此无法给出准确的各批次油品位置、批次间混油量与混油浓度分布、精确的批次注入或分输等操作计划。这影响了模型及其结果的准确性和可靠性。

2 热油管道非稳态水力与热力问题研究只集中于原油管道

埋地管道与其周围土壤温度场之间存在着传热且关系密切,因而有必要准确预测管道及其周围土壤的温度场。早期学者主要对热油管道非稳态土壤温度变化规律进行研究。计算埋地管道及其周围土壤温度场的方法主要包括解析解法、数值解法和经验公式法等。早期研究者将管道简化为一维模型计算

沿线温降,近年来研究者在此基础上沿管道轴向每隔一定距离取一个二维截面计算管道与大地的传热,实现从一维问题到拟二维问题的跃升。

沿线一维模型的解析法包括线热源法^[27]、当量环法^[27]、温度叠加法^[28],截面二维模型的解析法包括保角变换法和拉普拉斯变换法^[29~32],但解析解的形式过于烦琐且假设条件较多,不便于工程应用。用半解析法、或数值法求解热油管道一维非稳态流动与二维非稳态传热耦合问题时,需要结合具体的工程问题。研究者通常都采用一维非稳态的连续性方程、动量方程、能量方程,以及状态方程、定解条件、管道形变与温度和压力的关联式,对管内热油流动与土壤间的传热进行描述,然后再在必要的假设基础上,对方程组作适当简化^[27,33]以降低求解难度,最后通过半解析法或数值法进行求解得出管道沿线的速度、压力、温度和密度等的分布。

如李长俊等人^[34]、邓松圣^[35,36]和崔慧^[37,38]考虑热油管道对其周围土壤温度场的影响和管道截面的半无穷大土壤区域的传热,通过半解析法对热油管道顺序输送过程中的水力、热力瞬变过程进行了分析计算,提出了描述冻土区土壤融化圈变化、非稳态工况传热与流动双层耦合的数学模型,通过一定的数学处理得到计算区域特征线方程,并采用有限差分法、双特征线法或有限元法进行了求解。而吴国忠等人^[39]、李伟等人^[40,41]、孙楠^[42]和张静等人^[43]将大地半无限大区域简化为划分为两部分的有界的矩形区域,考虑大气温度波动、不同季节气候、不同埋深条件下的土壤温度非稳态变化过程,用有限差分、有限元方法或ANSYS有限元软件等数值方法模拟出整个运行周期中管道周围土壤温度分布、加热站加热功率、沿线输送介质的温度分布等。

而卢涛等人^[44]、崔秀国等人^[45,46]、丁芝来等人^[47]、王凯等人^[48,49]、施雯等人^[50]、周诗崇^[51]、周建等人^[52]、范海成^[53]、姚峰^[54]、夏庆春^[55]、鹿广辉^[56]、宇波等人^[57,58]和Barley^[59]则还考虑了管内热油流变特性、凝固潜热、液凝固油区划分、包含分输的热油顺序输送,建立了架空热油管道与空气、埋地管道管内油流换热与管外土壤导热相互耦合的传热模型、双管同沟敷设的传热模型,运用热力特征线法、水力热力双特征线法、热力特征线与有限单元法相结合、热力特征线法与有限容积法相结合、有限差分与有限容积法相结合的数值方法,求解得出土壤温度场、土壤

与管内油流的换热量、轴向油流温度分布,并分析了出站温度、流量及压力、地温变化、原油物性、土壤物性、原油油品种类数、批次数、批次量、排列次序、分输比例和分输时间对管道设计阶段和运行阶段的成品油顺序输送混油的影响。但以上研究止于原油管道,未对成品油管道的热力问题进行研究,同时,研究时将油品沿管道的轴向流动简化为一维模型,一维混油模型不够精确,无法完整体现传热传质的耦合过程。研究者们的重点在于探究管外的土壤和大气温度场对管线温度的影响,因此未对也无法对批次油品间的混油问题、温度对混油问题的影响进行二维研究。

3 考虑温度对混油形成机理影响的研究现状

无论原油或成品油,对于无隔离设备的顺序输送管道^[60,61],混油均是不同种类油品在流动过程中产生的热量传递、质量传递和动量传递的综合作用结果。混油形成基于对流传递和扩散传递。对流传递由管截面速度场不均匀所致,混油在轴向上不断伸展。扩散传递包括分子扩散和湍流扩散,按扩散方向又可分为轴向扩散和径向扩散。分子扩散是由分子的微观运动引起,区域内物质的浓度差越大则分子扩散的强度也越大。湍流扩散是由流体微团涡旋引起的,湍流程度越大则湍流扩散作用越明显。湍流中涡流扩散作用的大小取决于湍流的强度,而湍流的强度又与油流中物质的分布有关,二者相互影响。湍流扩散比分子扩散大约一个数量级,且由于湍流脉动径向扩散比轴向扩散更显著,使油品沿管道截面均匀分布,因此在一定程度上径向扩散阻碍了混油的轴向伸展,从而湍流时产生的混油量远远小于层流时。

由于混油机理的复杂性和各条管道本身的特殊性,至今还没有被大家广泛接受的混油量的通用计算模型^[62,63]。目前,成品油实际运行管理中混油量的计算模型大多数是基于一维对称浓度扩散理论建立的^[64~67]。一维模型假定沿管道截面速度和浓度均匀分布,根据质量守恒和Fick扩散定律得到混油浓度和混油长度的解析式,并经实验修正相关系数,得到混油量的半理论半经验计算式^[68,69]。此外则采用纯经验公式,如Austin-Palfrey公式^[70]及其变管径条件下的修正式^[71],又如将混油段看作清管器状^[72],混油体积只与雷诺数、摩阻系数及管长有关,关于各种计算混油的经验公式可以参考文献^[73~77]。

混油的二维理论模型相对于一维理论复杂得多以致无法求出解析解^[78],因此有学者^[79]用CFD软件建模和求解,其中还增加了湍流模型。二维模型^[68,80-82]虽然复杂,但二维对流扩散混油理论能更加准确地刻画混油段的拖尾现象。混油段的拖尾现象是指从轴向浓度分布看,截面平均浓度分布曲线关于50%浓度截面并非对称^[68],汽油推动柴油时是混油头短,混油尾长。此现象最先由Netchval等人^[83]报道,后由Austin等人^[70]和Haisan^[84]在现场实验中证实。后来常福宣等人^[85]指出可用分数阶的对流-扩散方程来表达广义的Fick扩散定律,这种用分数阶微积分方程刻画的非局域性或非时域性的扩散现象称为反常扩散^[86],是对传统的Fick扩散定律的推广。反常扩散考虑了整个扩散过程的时间相关性和空间相关性,即流量与不同空间点的粒子浓度有关、浓度的变化历史与初始时刻的浓度有关。分数阶微分与反常扩散本质上是相似的,分数阶方程的分布曲线能更好地描述不对称的偏态分布,即尾部存在“拖尾”效应。时间分数阶阶数值越小,时间相关性越强,物质扩散速度越慢,拖尾现象越明显。而空间相关性使得扩散过程加快,即随着空间分数阶阶数值的减小扩散速度加快。目前对混油界面的非对称现象以及相关的反常扩散现象的研究尚不完善。商鹏^[87]研究低温顺序输送5号柴油时指出低温结蜡是造成大量混油的原因,前行油品在管壁结蜡,后行油品溶蜡过程造成了混油尾拖长现象。由此可见研究温度对反常扩散现象的影响是很有必要的。

无论一维或二维混油模型,模型中的有效扩散系数的准确程度直接影响混油量计算结果的准确性,有效扩散系数最先由Taylor^[64]提出,后由许多研究者完善,但他们提出的影响有效扩散系数的因素不尽相同。文献中研究的影响有效扩散系数的因素包括:管道管长与管径^[45,73,76,88,89]、流体的平均速度与速度随时间的变化^[65,73,88-96]、雷诺数变化与流态^[65,72,73,76,88-99]、油品的扩散浓度与浓度梯度^[45,73,76,100,101]、油品的相对压力^[102]、平均浓度与浓度随时间的变化^[64,73,76,83,88,98,103-107]、*Peclet*数^[62,98,100,103]、*Schmidt*数^[65,73,90-96,100]、*Froude*数^[45,73,101]、黏度扩散系数与湍流扩散系数^[62,65,79-81,90-93,96,97,100,108]、混油段与管壁间的摩擦系数^[72,73,80,81]、黏度边界层与紊流核心区^[79-81,96,97,100]、外力扰动如泵的频繁启停^[109]。以上研究均未考虑温度对有效扩散系数的直接影响。

顺序输送管路由于所处区域及环境温度的不同,它不能完全等同于等温管道^[1]。如Augusto^[110]指出在温度较低的轻质油后面紧接着输送温度较高的重质油时可以观察到温度的瞬变效应。夏季管内油品常常高于地温,冬季管内油品常接近于埋深处的地温。随着温度不同,油品的物性如密度、黏度会发生变化^[111,112],会导致管截面上局部流速分布不均和油品扩散系数的改变,从而影响管道横截面上的油品浓度分布,导致油品交替时混油量的变化,对于大口径长输管道更是如此^[113]。文献[100]根据半经验的湍流理论建立了考虑交变温度因素的流速断面,考虑交变黏度和密度的管中湍流双层系统,从而确定非等温流中的有效扩散系数,以此分析温度变化对混油过程的影响。但其是将温度的影响引入黏温关系曲线中^[5,89],温度是通过影响黏度间接影响有效扩散系数的。在层流区如此,而在湍流区是考虑温度对雷诺数的影响,对混油区雷诺数增加一个指数形式的修正项,也是间接影响有效扩散系数。文献[100]还进一步指出温度对动量和物质传递过程的影响主要存在于层流边界层,因为边界层区相对于湍流核心区而言失去了湍流脉动特性,传质过程以分子特征呈现。Riazi等人^[102]把密度与有效扩散系数的乘积看作一个整体称为等效扩散系数,指出其与两种流体的相对压力、黏度比、相对温度、分子质量以及压缩因子有关,其适用于气液两相系统、非烃类系统甚至三元系统,且适用的压力范围较大。但其需要通过实验测定部分参数且误差较大,主要适用于油气藏开采时的两种流体混合过程。

4 温度对管输成品油过程流动传质影响的研究现状

4.1 温度影响引出的问题

温度对管输过程的影响本质是管输油品存在可压缩性和膨胀性,在不同的温度条件下,油品的物性沿管道轴向和径向分布不均匀并随着外部环境变化而变化。影响主要体现在以下几个方面:(1)输量变化^[33]。油品温升使煤油、柴油等燃料油的黏度降低,站间的摩阻也相对减小,这将缩小输送燃料油与输送汽油之间耗用动力的差异,且黏度和密度降低还可以增加全线的输量,这是油品升温的有利方面。(2)油品过泵或节流后的温度升高可能产生汽化现象,

出现计量误差,还会使管道产生热膨胀,出现安全隐患。(3) 成品油管道的管容与所输送油品体积受温度的影响,从而影响油品批次界面跟踪的准确性。国内现用的成品油管道优化运行软件在进行油品调度和批次跟踪时给出的水力模拟结果与现场存在误差,原因是没考虑温度的影响^[1]。各批次油品的到站时间因受到温度影响的不同,存在提早或推迟的差异^[1,114]。(4) 混油量及混油分布计算不准确影响混油切割的准确性^[1,4]。(5) 温度降低也是造成成品油管道停输后出现管道压力降低的主要原因^[115]。(6) 温度较高的油品进罐后,轻质组分蒸发量增大,导致油品质量损失增大。蒸发损耗还会加速汽油氧化,增加胶质,降低辛烷值^[116]。

4.2 针对温度影响的理论研究

要解决温度的影响问题,就需根据安排的油品批次,掌握沿线管内纯油和混油的体积、位置及分布情况。早期学者^[100]对沿线温度变化下的顺序输送的混油进行研究时,沿线的温度分布采用稳态热油管道计算公式(苏霍夫公式)确定,同时通过黏温指数关系表示油品黏度随温度的变化,且紊流扩散系数与扩散浓度无关。之后考虑温度与流动、传质的耦合,用连续性方程、动量方程及能管内油量方程对非稳态流动与传热进行描述^[45,48,59,68,117,118],用一维或二维的非稳态对流扩散方程描述混油的形成与发展过程^[33,36,63,68,69,113,119],部分学者还增加了描述湍流的 $k-\varepsilon$ 模型^[79]。对此偏微分方程组进行求解,一是确定边界条件与初始条件使其封闭,二是处理其耦合性。在建立定解条件使方程组封闭方面,主要问题是对总传热系数^[36,63,113,119]、有效扩散系数^[45,100]、雷诺数等特征数^[100]、流体状态方程和管壁方程^[59,118]以及边界层效应^[36,63,68,69,80,97,113,119]的建模和计算,不同学者建立不同的模型描述这些关键量之间及与待求变量之间的关系,部分学者还考虑了纯油品的物性参数与温度和压力的关系^[45,100]及计算混油物性的混合法则^[73,100]。在处理模型的耦合性方面,不同的学者在各自建立的假设基础上对方程组进行适当简化再求解,一是将非稳态问题近似为稳态问题^[36,63,113,119],二是将耦合性强的项进行适当简化再用数值^[45,59,68,69]或半数^[33,36,63,113,119]的办法求解,三是直接利用商业CFD软件进行数值模拟^[68,69,79],利用其内嵌的经验公式。

可以看出,目前在三维下理论研究还未开始,二维下模型的耦合性处理还不完善。同时,混油模型也未考虑到反常扩散现象,湍流对传质影响的微观机理也尚未得到揭示,管内外温度场的耦合考虑得也不够具体。也尚未考虑油品的可压缩性,管输设备如泵和阀门对油品物性参数及混合规则的影响。因此考虑温度影响的计算方法还需进一步完善和发展。

4.3 实践中消除温度不利影响的方法

科洛尼尔管道^[120]在输量增大后出现了油品温升问题,随之而来的一系列上述问题促使其研究从低输量到高输量变化全过程中油品温升变化,经过计算和现场获得的数据,通过建立数据库的方式并利用统计学理论取得了一种可以预测全线各点油温的方法。邓松圣等人^[121]对成品油站内温升、节流温升和站间温升的机理进行了分析并给出了油品温升的计算公式。其后^[116]又对利用河水冷却管道和制冷冷却两种降低油品温度的措施进行了研究,提出了强迫对流方式降低油品温度的设计计算方法。崔艳雨等人^[122]研究温度对油品体积和管容、压力对油品体积和管容的影响,引入体积压缩系数及温度膨胀系数得到计算界面位置和提高批次跟踪准确度的方法。郭伟等人^[123]认为油品温度的降低是港枣成品油管道停输后管内压力出现平滑下降的主要原因。其后文献^[4]又在计算油品批次在管中位置时,引入温差修正了混油段中间位置界面距离上游站的里程,通过逐站修正混油界面位置的方法提高界面跟踪的精度。张运雷等人^[5]在郭伟的基础上又将温度对油品黏度的影响加入到混油量的计算和对混油界面位置的修正计算中,其后郭伟等人^[4]分析了西部成品油管道混油切割量显著攀升的原因,提出采取改变切割比例、修正密度偏差、改变首站油品切换模式等措施降低混油切割量。梁永图等人^[1,114]计算了输送周期内管道沿线温度的变化,考虑摩擦生热、大地换热、站内节流、过泵导致的温度变化,给出了与温度相关的计算批次界面位置的修正系数。

但目前模拟类方法尚停留在理论研究阶段,修正类方法误差仍然较大,现场应用效果不够理想。故需进一步对温度的影响及其耦合机制进行研究,改进沿线各站收发油品、检测油品浓度分布、计算混油量、切割和处理的手段,以保证顺利完成油品的储运作业^[124]。

5 实验研究温度对管输成品油的影响

无论是搭建室内实验环道还是在工业管道上, 均已研究者对成品油的顺序输送过程进行了相关的实验研究. 研究着眼于发现混油段以及给出计算混油量的经验公式, 集中于流态、油品种类、管道参数对混油量的影响, 尚未考虑温度在其中的作用和影响机制.

1943年, 研究者Fowler和Brown^[125]用物性几乎相同的水和稀释的NaCl溶液在管径0.124和0.313 in (1 in=2.54 cm), 管长从5~105 ft (1 ft=30.48 cm) 的玻璃管中进行顺序输送试验, 试验管长和管径之比从低于200~10000, 雷诺数从低于200~19800. 商业管道输送的油品黏度从0.51~7.4 cst (1 cst=1 mm²/s), 对应雷诺数范围为27000~610000 (平均雷诺数为55000~537000), 管长和管径的比率从437000增大到1765000. 根据实验室和商业管道的混油数据, 他们做出混油体积占管道体积百分数与雷诺数、混油浓度范围两者的关系图, 得出结果是层流时混油体积与雷诺数无关; 湍流时雷诺数增大混油量减少, 并总结出了与实际管道误差较小的混油体积计算公式.

壳牌石油公司研究者^[91]为研究成品油管道中油品混合特性, 建立了中等规模试验装置. 首先在20 ft 宽(约6.10 m), 90 ft 长(约27.43 m)的建筑物内, 用管内径0.6 in(约15.24 mm), 长5000 ft(约1524 m)的树脂管(saran tubing), 围绕建筑物的内屋檐连接成试验管道. 增压装置为1台叶轮泵, 其变速驱动装置可连续提供每分钟600转到3600转的变速. 测量装置是1台1 in的活塞式流量计. 试验操作流速下, 雷诺数最高能达到200000. 在树脂管线完成了一些试验之后, 为了能与现场管道更接近, 因此又建设了一个新管道系统^[92]. 该系统包括管径2 in, 管长5000 ft的焊接钢管和新的更大的泵送装置、测量装置和比重计. 该环道的设计包括了必要的阀室和管件, 可以发放隔离器以便研究油品隔离的方法. 增压设备为2台旋转泵, 泵可提供每分钟600~3600转的变速增压. 测量装置是1台2 in的旋转流量计. 三个油罐与系统相连. 系统中还有压力表、温度计插孔等, 以便在每次试验中获得完全的试验数据. 试验流体包括丙烷、丁烷、汽油、煤油和燃料油. 实验流速从0.44~7.16 m/s, 雷诺数从500~195500. 实验管道长度也随试验流动的运行条件和流体粘度变化, 从50000 ft变化到300000 ft. 在0.6和2 in的试验管线上共完成了250多个混油试

验^[126]. 基于混油试验结果, 总结得到了雷诺数大于20000时的混油长度经验公式.

Hara等人^[127]报道安装在Keihin工厂的管径4 in、管长1300 m的试验管线上顺序输送车用汽油和煤油的混油试验, 但是没有详细报道相关工艺.

1980年^[128], 中国在一条长55 km, 地形比较复杂, 最大高差为850 m, 途径4个泵站的野战输油管线上进行了汽油-航空煤油的顺序输送工业性试验, 试验时在收油库的计量站及离油库3 km的上游设1台超声波油品检测仪, 用以测量预报混油段, 当混油段到达计量站时, 每3 min抽检一次油样, 对其密度、闪点、干点等进行化验, 结果发现航空煤油中含的汽油超过1%时, 其闪点不合格, 汽油中含航空煤油超出3%时, 其干点不合格. 1984年^[128], 中国又在一条长110 km有6个泵站的输油管线上顺序输送了汽油-柴油-航空煤油, 利用超声波油品检测仪测量了混油率, 汽油和柴油的为0.93%, 柴油和航空煤油的为1.82%.

Luyeri^[100]在室内建立了一套实验环道, 顺序输送水和0.1当量(4 g/L)的NaOH水溶液, 实验在管径为58 mm, 长60 m的玻璃管道内进行. 通过测量导电性来确定一种液体在另一种液体中的浓度, 通过测量检测到的混合液段流动的持续时间来计算混合液段的长度和体积. 混合液段流动的持续时间是, 从管中心处传感器附近浓度开始变化的瞬间开始, 到管壁处传感器附近浓度开始变化的瞬间为止的时间间隔. 实验研究了两种溶液的不同输送顺序、不同流动状态对此时间间隔的影响, 并据此进一步分析影响混合液尾端长度的因素, 影响有效扩散系数的因素. 同时在该实验系统上进行了盲肠管冲刷等复杂边界条件的实验研究, 通过理论分析和实验修正建立了相应的混合液体积计算公式.

Freitas等人^[73]建设了一套顺序输送实验环道, 用安装在末站处的采样频率为0.2 Hz的超声波流量计通过监测混油段的声速的办法来记录混油段长度的发展过程. 并将采集的实验数据与自己建立的模型^[129~131]以及几种常用预测混油量的方法^[70,76,83,91,92,104~106]的结果进行了比较. 在2%~98%浓度范围内其建立的模型的预测结果与试验结果最接近. 并且在后来的研究中, 简化了其采用的轴向有效分散系数与雷诺数的关系式.

康正凌^[132]通过分析相邻油品的密度差和黏度差对混油过程的影响后, 推导了与混油区的物质分布

相关的轴向有效扩散系数,提出了管道顺序输送高差混油模型.在此基础上,通过对自行设计建设管长为165 m,管径为2 in(内径为51.44 mm)的无缝镀锌钢管的高差混油实验系统进行混油实验.对照1974年的顺序输送工业试验数据,以及对兰成渝成品油管道现场高差混油试验的分析和讨论,认为摩阻系数实际值与理论计算值的偏差是影响混油理论预测值的重要因素.

耿德江等人^[133]设计一个小型管流蜡沉积试验装置,研究高凝成品油在低地温管道顺序输送时管壁的结蜡规律,发现较高的出站温度下降到与地温基本相同时易产生结蜡,建议尽量提高流速或输油温度以减少前行油品蜡的沉积,防止产生更多混油.

潘振^[126]提出基于V锥流量计压力差信号的成品油管道顺序输送混油界面检测方法,利用稠化水与水、盐水与水分别模拟两组不同油品在顺序输送环道中的流动,研究了不同黏度和密度对V锥流量计压力差信号的影响,但未研究温度对流体物性及压力信号的影响.

在以上前人做的实验中,仅壳牌公司所做的顺序输送混油特性试验中进行了一些节点的压力和温度的监测,但是在分析实验结果的过程中并没有结合温度考虑其对混油的影响.而其他学者所做的实验研究均没有对顺序输送实验过程中的温度进行监测,也即目前所有的顺序输送混油计算方法和进行的顺序输送混油实验都未考虑温度、压力等因素对混油的影响,未深入探究管内外流动、传热和传质规律.

6 结论及建议

顺序输送时管道的水力特性、混油产生过程、批次界面检测与切割、调度计划制定与实施、泄漏检测与事故处理均与油品的种类和物性密切相关,所以获得准确的油品物性参数的时空分布十分关键.而管内油品物性的时空分布又与油品温度、压力等状态参数分布相关,因此在管道的设计、运行、管理和优化的离线仿真中,应充分考虑油品温度、压力变化的

影响,采取相应的措施确保批次油品的状态参数和物性参数能够快速准确获取,进而获得其他参量的准确分布.因此尚有以下几个方面需要进一步研究:

(1) 将成品油管道调度与水力进行耦合的研究较少,考虑温度的影响即与热力耦合的研究则更少,在向枝状管网甚至环状管网发展的趋势下,批次界面的快速准确跟踪及检测显得更加重要,考虑温度影响的调度模型及算法亟需深入研究.

(2) 针对混油拖尾现象的理论和实验研究均不完善,针对混油界面的非对称特性的研究也不够深入,以油品品质或质量潜力为指标的批次界面跟踪更是刚刚起步,而温度在此过程中的作用尚未探明,因此在油品反常扩散现象、混合机理以及混油发展过程中更全面更深入地考虑温度的影响需要进一步研究.

(3) 目前求解管输成品油的水力-热力-混油耦合模型的方法均假设了油品不可压缩,而考虑温度的影响时必须考虑油品及管道所具有压缩性和膨胀性,同时,实际生产中的管输成品油均为紊流状态,因此如何对可压缩、多组分、紊流流体流动现象进行建模以及开发相应的稳健性好、计算效率高的算法是未来的研究方向之一.

(4) 顺序输送的长输管道内的流动、换热和混油的耦合数值模拟尚停留在拟二维阶段,数字化和智能化管道平台要求对三维管道进行更逼真的模拟和跟踪,以作为后续的优化停输、泄漏检测、泄漏过程模拟、泄漏量计算等的基础.因此进一步在三维坐标系下研究混油规律,以及对长数千千米的长输管道内的流动传热整体进行数值模拟并保证模拟区域内计算数据的连续性是将需解决的问题.

(5) 复杂条件下的管道建设是发展趋势,如冻土区、深海区等,同时设备升级、油品种类增加、输送工艺改变、工况增加等都会为流动、传热和传质耦合模型的定解条件产生影响,为数值模拟增加难度.因此如何建立及求解包含多种、多个复杂边界条件的成品油流动传热传质及批次跟踪综合方程组将是今后该领域的研究重点.

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Summary for “温度对成品油管道顺序输送过程的影响研究进展”

Research advances in the influence of temperature on the sequential transportation in product pipeline

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Sequential transportation is the main way of long-distance transportation for the oil product, whose essence is a coupling process of flow, mass transfer and heat transfer. Thus, like the pressure gradient and the concentration gradient, the heat gradient is one main power source of the mentioned coupling process as well. The previous related study done by researchers both at home and abroad mainly focus on the aspects including the making scheduling plans for batches in the oil product pipeline, the oil batch interface tracking as well as simulation, the scheme optimization for activating pumps, the mechanism of forming mixed oil and the detection of oil leakage. However, all of these works have failed to take the proper factor of temperature into consideration. As for the researches on experiments, the majority of them concentrate on factors such as the flow patterns, the categories of the oil product, and the parameters of the pipeline and on those factors' influence upon the total amount of the mixed oil. They all have been irrespective of the effect of temperature and corresponding mechanism. Most of the researches regard the pipeline as an isothermal body, which is a postulated condition in their papers. In the background of digital pipeline system and intelligentized management transportation system, both of a better accuracy and reliability are required for the model to deal with the problem mentioned above. Thus, the classical theory regarding mixed oil, coupling of flow and heat transfer, scheduling plans, separation of mixed oil and leakage detection cannot keep up with the pace the development of the pipeline system. At present, researches of the following aspects are in a fledging period: the smearing phenomenon of mixed oil, the scheduling plans making considering nonlinear factors, the scheduling plan optimization considering coupling of hydraulic and thermal factors, the batch interface tracking regarding the oil quality and the three-dimensional transient flow simulation in long-distance pipeline, which need to make a further study shedding light on the detailed mechanism concerning the temperature's influence. Thus, firstly in the paper, the correlated researches on mixed oil, scheduling plans, heated oil pipelines and batch interface tracking without taking temperature's influence into account have been summarized and the corresponding defect has been discussed. Next, current status of researches about the temperature's influence on the mechanism of mixed oil and on the process of mass transfer as well as heat transfer are analyzed and commented, including the related experimental research. The influences are embodied in the change of transport capacity, the vaporization of oil, the decreasing quality of oil, the low accuracy of batch interface tracking, the high risk of mixed oil cutting and the large pressure drop after pipeline shutdown. Correspondingly, the relevant theoretical and experimental studies are not perfect and sufficient. And the empirical formulae or modified coefficient methods presented in these studies are not suitable enough for the industrial applications. At the end of the paper, it is pointed out that based on the development requirements of the pipeline system, the scheduling plan combined with thermal as well as hydraulic factors, the abnormal diffusion considering temperature between different batches, the three-dimensional simulation of compressible multi-phase turbulence and the batch interface tracking in complex pipelines are the major research directions and key issues in the research field.

sequential transportation, temperature, batch interface tracking, mixed oil, mass and heat transfer coupling

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